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FEASIBILITY STUDY OF A QUADRILATERALIZED SPHERICAL CUBE EARTH DATA BASE

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N O T I C E

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes the results of research into the feasibility of storing satellite meteorological data in a high-resolution, equal-area, computer-accessible data base. Equal area elements are stored in square arrays representing the faces of a cube inscribed within the Earth. The required area-preserving transformation is presented along with its inverse. A unique array-mapping scheme is presented, which preserves near-neighbor relations and allows rapid index computation. The implementation of this data base on rotational storage devices is discussed, and calculated execution times are presented.		

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EXECUTIVE SUMMARY

This report presents the results of a feasibility study of the Quadrilateralized Spherical Cube Earth Data Base. The structure of this data base is derived from a spherical cube, which is obtained by radially projecting a cube onto its circumscribing sphere. An appropriate set of curvilinear coordinates is chosen such that the resolution cells on the spherical cube are of equal area and are also of essentially the same shape. This geometrical construction eliminates both the necessity to account for nonequal-area cells, and the need to compute the location of every cell in the data base.

The main properties of the Earth data base are as follows:

1. The indexing scheme is binary in nature, and telescopic in the sense that each additional level of resolution is addressed by appending additional binary bits. Thus, minimal work is needed for indexing cells of higher resolution.
2. The resolution cells are strung together in a two-dimensional manner, so as to accomplish area coverage with a serial bit string. Consequently, a higher degree of proximity is achieved for near-neighbors in this stringing pattern than in the usual one-dimensional array of stringing by rows and columns.
3. The cell addresses are readily computed because of the indexing scheme which is the same regardless of the resolution level, and because of the stringing pattern which permits the decomposition of the cell address into two independent binary indices.
4. The conversion from geographic coordinates to data base coordinates is comparatively simple because of the simplicity of the data base structure.

5. Incoming data can be stored rapidly by interpolation, using benchmarks only occasionally. This method of fast-filling is made possible by the equal-area nature and translational shape invariance of the data base resolution cells.
6. Input/output operations with this data base are also simplified because of the rectangularized nature of the data base records and the rhombic nature of the interpolation blocks.
7. The user can rapidly and directly access data corresponding to specified geographic regions of arbitrary shape and size. This data-accessing is accomplished by retrieving the relatively few bit-strings which lie within the associated data base records. The rapidity and directness of data access are the result of equal-area resolution, translational invariance, indexing scheme, stringing pattern, and relatively simple coordinate transformation.
8. The primary contemplated uses of the retrieved data are mathematical computations and visual display. For the former, the equal-area resolution property eliminates the need to distinguish between density measurements and integrated measurements. For the latter, the quadrilateralized nature of the resolution cells on the spherical cube and the comparative simplicity of coordinate transformation both simplify and minimize the internal operations.

Based on numerical results obtained in this study, it is concluded that implementation of the proposed Quadrilateralized Spherical Cube Earth Data Base is feasible on current large-scale computer systems.

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SECTION 1 - INTRODUCTION

In the numerous satellites presently orbiting the Earth, enormous amounts of data are continuously taken of the Earth's surface and atmosphere. These data are of a varied nature: topography, crop distribution, sea surface temperature, cloud coverage, etc. The measurements are used by research and applications personnel of diverse scientific disciplines. These users usually employ an Earth-oriented coordinate system, such as the traditional geographic frame of reference. Thus, it is not surprising that almost all existing Earth data bases have been constructed with latitudes and longitudes as grid-lines, either in a patched-up partial fashion or in the entire outlay.

However, what is convenient to the user is not necessarily also efficient from the standpoint of data management and data processing by the computer. Efficiency is especially important because of the large amounts of data rapidly acquired in global coverage, the necessity to update data continually for operational use, and the desire to access directly relatively small amounts of data corresponding to selected geographic regions at appropriate times.

The high computer overhead encountered in processing can therefore be minimized by designing an Earth data base structure with constant (but selectable) geometric resolution cells, which are also locally invariant in shape along a translation in any direction. This would eliminate the necessity to account for nonequal-area resolution cells, and also the need to compute the location of every resolution cell in the data base. Moreover, the design should also utilize a fairly simple transformation between the user-preferred geographic coordinates and the internal data base coordinates. This would greatly facilitate arithmetic and transfer operations desired by the user in mathematical computations or in graphic display.

In the previous study (Reference 1), six data base structures were conceptualized. Of these, the most promising was the Quadrilateralized Spherical Cube Data Base. In this model, the sphere is visualized as a spherical cube, as illustrated in Figure 1-1. This spherical cube is obtained by radially projecting the edges of an inscribed cube, as shown in Figure 1-2.

From Figure 1-2, it is obvious that equal-area elements on the plane square do not radially project as equal-area elements on the spherical square. For example, those elements near the center of the plane square have larger projections than those elements near the edges of the plane square. Hence, if a rectangular grid of equal-area elements is first constructed on the plane square, it is then necessary to distort this grid into a curvilinear network so that the elements near the center are smaller than those near the edges. The distortion is such that when the curvilinear elements are projected radially, equal-area elements are again obtained on the spherical square. The desired sequence of transformations is illustrated in Figure 1-3 through 1-5. The mathematical details of deriving these transformations are discussed in Section 2.

For the present, it suffices to say that it is possible to obtain a world map such as Figure 1-6. This map illustrates the continental outlines as they would appear on the cube with the original undistorted rectangular coordinates. This is accomplished by reversing the sequence of transformations previously illustrated by Figures 1-3 through 1-5. Thus, in Figure 1-6, equal-area regions correspond to equal-area regions on the spherical Earth. An examination of this planar equal-area world map shows that the distortion of the continental outlines is not as great as might be expected.

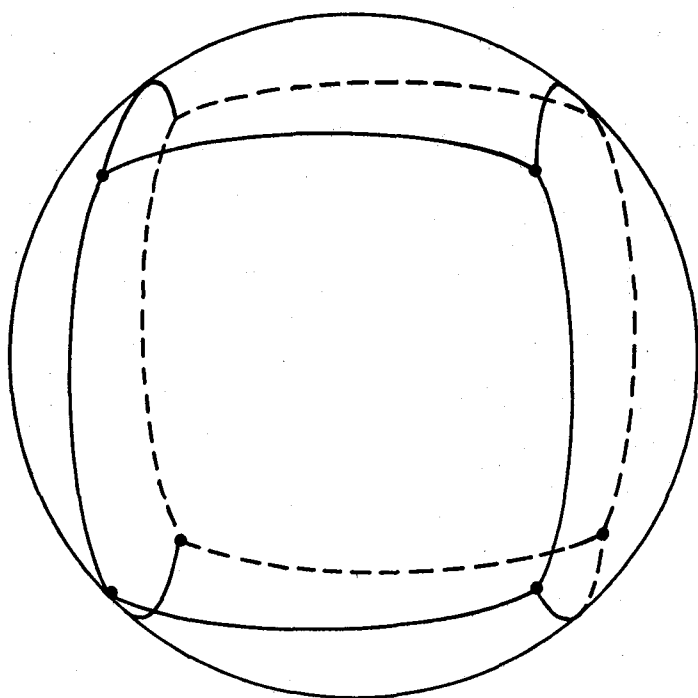


Figure 1-1. Spherical Cube

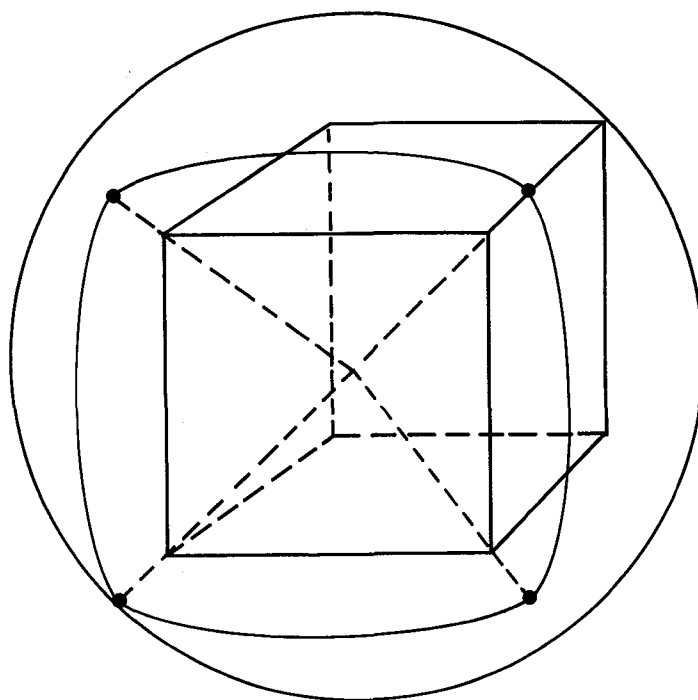


Figure 1-2. Construction of the Spherical Cube

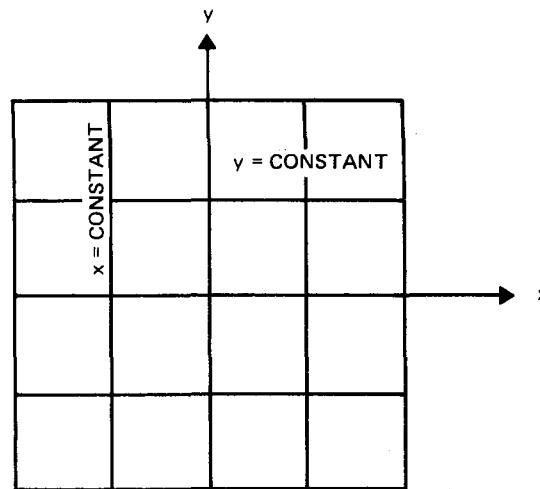


Figure 1-3. Plane Square With Cartesian Coordinates

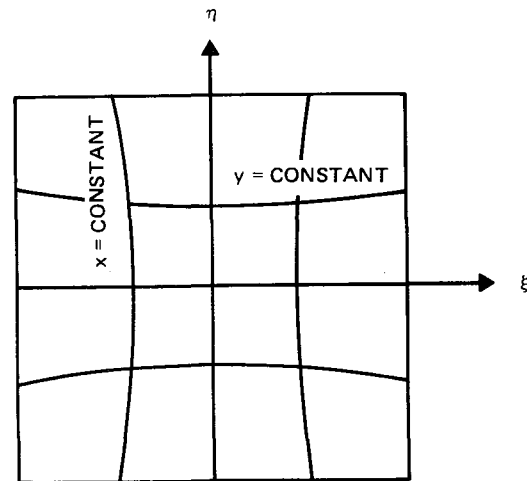


Figure 1-4. Plane Square With Curvilinear Coordinates

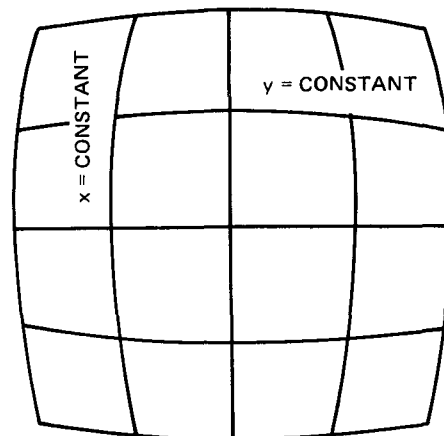


Figure 1-5. Spherical Square With Curvilinear Coordinates

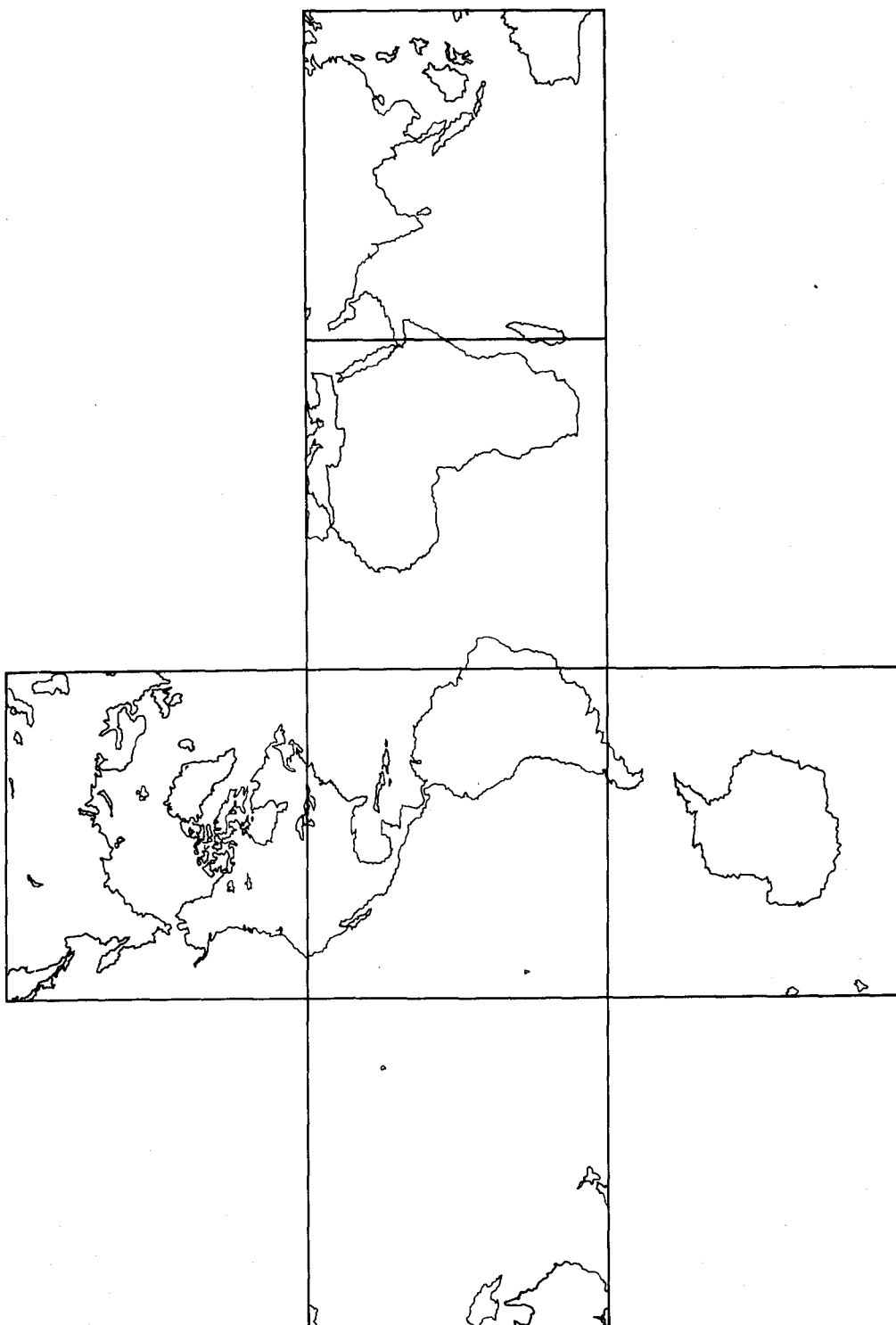


Figure 1-6. World Map on Equal-Area Cube

SECTION 2 - MATHEMATICAL FORMULATION OF DATA BASE STRUCTURE

2.1 SUMMARY

This section is concerned with the derivation of a mapping function which leads to the division of a spherical cube into quadrilaterals of equal area. Specifically, the method involves: (1) dividing a plane square into rectangles of equal area; (2) transforming the rectangular coordinate system on the plane square to a curvilinear coordinate system on the same plane square; and (3) projecting the new nonequal-area elements on the original plane square to a subtending spherical surface such that equal-area spherical surface elements are again obtained. In addition to the direct transformation function described, analysis is also performed for obtaining the inverse transformation function which reverses the above process.

2.2 DERIVATION OF DIRECT MAPPING FUNCTION

First, consider a plane surface subtended by a spherical surface with radius R . Let \vec{r}_o be the vector from the center of the sphere to the given plane. As shown in Figure 2-1, let dA_p be an area element on this plane, and let \vec{r} be the vector from the center of the sphere to the area element dA_p .

Let dA_s be the spherical area element obtained by projecting dA_p radially onto the sphere. Then, it can be readily shown that the following relation between dA_p and dA_s holds:

$$dA_s = \frac{R^2 \cos^3 (\vec{r}, \vec{r}_o)}{r_o^2} dA_p \quad (2-1)$$

where (\vec{r}, \vec{r}_o) denotes the angle between \vec{r} and \vec{r}_o .

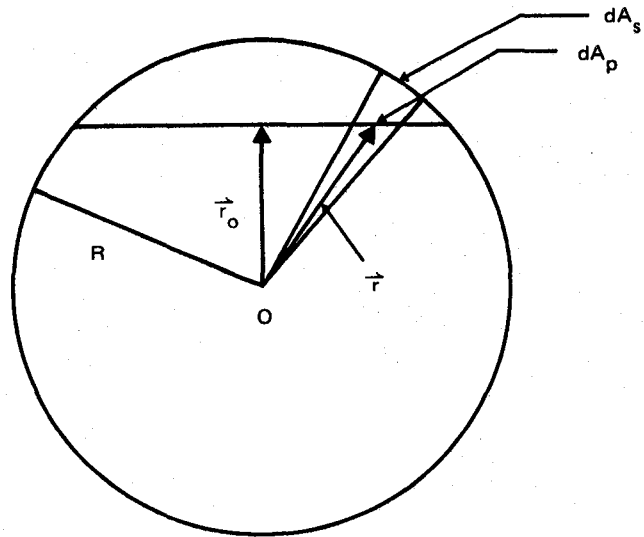


Figure 2-1. Relation Between Plane and Spherical Area Elements

Let (ξ, η, r_0) denote the components of the vector \vec{r} . Then, it follows that

$$\cos(\vec{r}, \vec{r}_0) = \frac{r_0}{r} = \frac{r_0}{(r_0^2 + \xi^2 + \eta^2)^{1/2}} \quad (2-2)$$

Moreover, for convenience, let the unit of length be chosen such that the radius, R , of the sphere is equal to unity. Then, Equations (2-1) and (2-2) yield

$$dA_s = \frac{r_0}{(r_0^2 + \xi^2 + \eta^2)^{3/2}} dA_p \quad (2-3)$$

Next, consider a cube together with a circumscribing spherical surface. On each of the six plane faces of the cube, a rectangular coordinate system (x, y) may be defined, the domain of definition being $-r_0 \leq x, y \leq r_0$. It may be easily verified that

$$r_0 = \frac{1}{\sqrt{3}} \quad (2-4)$$

Let a new coordinate system (ξ, η) be defined by

$$\begin{aligned} \xi &= \xi(x, y) \\ \eta &= \eta(x, y) \end{aligned} \quad (2-5)$$

where $\xi(x, y)$ and $\eta(x, y)$ are independent arbitrary functions.

The new area element $d\xi d\eta$ is related to the original area element $dx dy$ by

$$d\xi d\eta = J\left(\frac{\xi, \eta}{x, y}\right) dx dy \quad (2-6)$$

where $J\left(\frac{\xi, \eta}{x, y}\right)$ is the Jacobian of transformation

$$J\left(\frac{\xi, \eta}{x, y}\right) = \begin{vmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \xi}{\partial y} \\ \frac{\partial \eta}{\partial x} & \frac{\partial \eta}{\partial y} \end{vmatrix} \quad (2-7)$$

If this new area element is projected radially onto the surface of the sphere, Equations (2-3) and (2-6) yield

$$dA_s = \frac{r_o}{\left(r_o^2 + \xi^2 + \eta^2\right)^{3/2}} J\left(\frac{\xi, \eta}{x, y}\right) dx dy \quad (2-8)$$

which relates the spherical area element dA_s to the original area element $dx dy$. For original equal-area plane elements $dx dy$ to transform into equal-area spherical elements dA_s , it follows that

$$\frac{r_o}{\left(r_o^2 + \xi^2 + \eta^2\right)^{3/2}} J\left(\frac{\xi, \eta}{x, y}\right) = \lambda^2 \quad (2-9)$$

or

$$\frac{r_o}{\left(r_o^2 + \xi^2 + \eta^2\right)^{3/2}} \left(\frac{\partial \xi}{\partial x} \frac{\partial \eta}{\partial y} - \frac{\partial \xi}{\partial y} \frac{\partial \eta}{\partial x} \right) = \lambda^2 \quad (2-10)$$

where λ^2 is a constant.

It is easy to verify that the value of λ^2 is equal to the ratio of the area of the spherical square to the area of the plane square, i.e.,

$$\lambda^2 = \frac{2\pi/3}{4 r_o^2} = \frac{\pi}{2} \quad (2-11)$$

An alternative form of Equation (2-10) is

$$\frac{\partial \xi}{\partial x} \frac{\partial \eta}{\partial y} - \frac{\partial \xi}{\partial y} \frac{\partial \eta}{\partial x} = \gamma^2 \left(1 + \frac{\xi^2}{r_o^2} + \frac{\eta^2}{r_o^2} \right)^{3/2} \quad (2-12)$$

where

$$\gamma^2 = r_o^2 \lambda^2 = \frac{\pi}{6} \quad (2-13)$$

From Equations (2-7) and (2-12), it is seen that γ^2 may be interpreted as the area-scale of transformation at the point $(\xi = 0, \eta = 0)$.

Equation (2-12) in itself is quite general. It is now desirable to specify the following general properties for the transformation from (x, y) to (ξ, η) .

1. To preserve symmetry in the transformation Equation (2-5), it is required that

$$\begin{aligned}\xi &= f(x, y) \\ \eta &= f(y, x)\end{aligned}\tag{2-14}$$

Equation (2-14) states that ξ and η have exactly the same form of dependence on x and y , except that the roles of x and y are interchanged. Moreover, symmetry preservation also requires that the function $f(x, y)$ be odd in x and even in y , i.e.,

$$\begin{aligned}f(-x, y) &= -f(x, y) \\ f(x, -y) &= f(x, y)\end{aligned}\tag{2-15}$$

As a consequence of Equations (2-14) and (2-15), it is seen that the origin maps back into itself, i.e.,

$$f(0, y) = 0\tag{2-16}$$

2. To map points on the sides of the square back into points on the same sides, it is necessary that

$$f(r_o, y) = r_o\tag{2-17}$$

As a consequence of all the above requirements, it may be shown that $\frac{\partial \xi}{\partial y}$ and $\frac{\partial \eta}{\partial x}$ are zero at the points $(0, 0)$ and (r_o, r_o) . Therefore, from Equation (2-12), it follows that

$$\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=0 \\ y=0}} = \left. \frac{\partial \eta}{\partial y} \right|_{\substack{x=0 \\ y=0}} = \gamma = \sqrt{\frac{\pi}{6}} = 0.72360 \ 12545 \ 582 \quad (2-18)$$

$$\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=r_o \\ y=r_o}} = \left. \frac{\partial \eta}{\partial y} \right|_{\substack{x=r_o \\ y=r_o}} = \mu = \sqrt{\frac{\sqrt{3}\pi}{2}} = 1.6494 \ 54166 \ 187 \quad (2-19)$$

If $f(x, y)$ can be expanded in a power series in x and y , then Equation (2-16) requires that

$$f(x, y) = x \sum_{i=0}^{\infty} \sum_{j=0}^{\infty} a_{ij} x^{2i} y^{2j} \quad (2-20)$$

The condition in Equation (2-18) yields

$$a_{00} = \gamma \quad (2-21)$$

The condition in Equation (2-17) may be incorporated into $f(x, y)$ by writing it in the form

$$f(x, y) = \gamma x + \frac{(1-\gamma)}{2} x^3 + \left(r_o^2 - x^2 \right) x \sum_{(i+j) \geq 1} b_{ij} x^{2i} y^{2j} \quad (2-22)$$

It may be shown that Equation (2-12), together with the conditions given by Equations (2-16) through (2-18), are not sufficient to determine uniquely the transformation in Equation (2-14). This nonuniqueness is manifested by the fact that there are more unknowns (b_{ij}) than equations when Equation (2-22) is substituted into Equation (2-12) and terms of the same degree are equated. Finally, to incorporate the condition in Equation (2-19), it is most efficient to express $f(x, y)$ in the following form. The details for arriving at this form are given in Appendix A.

$$\begin{aligned}
 f(x, y) = & \gamma x + \frac{(1-\gamma)}{r_o^2} x^3 \\
 & + xy^2 \left(r_o^2 - x^2 \right) \left[\delta + \left(r_o^2 - y^2 \right) \sum_{j \geq 0} c_{ij} x^{2i} y^{2j} \right] \\
 & + x^3 \left(r_o^2 - x^2 \right) \left[\omega + \left(r_o^2 - x^2 \right) \sum_{i \geq 0} d_i x^{2i} \right]
 \end{aligned} \tag{2-23}$$

where

$$\begin{aligned}
 \delta = & \frac{1}{4r_o^4} \left[-(\mu + 2\gamma) + \sqrt{(\mu^2 - 4\mu\gamma + 4\gamma^2 + 16\sqrt{2}\gamma^2)} \right] \\
 = & 0.79048 \ 64491 \ 208
 \end{aligned} \tag{2-24}$$

$$\begin{aligned}
 \omega = & \frac{1}{2r_o^4} \left(3 - 2\gamma - \mu - 2r_o^4 \delta \right) \\
 = & -1.2254 \ 41487 \ 984
 \end{aligned} \tag{2-25}$$

An approximate mapping function may be obtained by truncating the series expansion in Equation (2-23) at some degree, and then obtaining the coefficients c_{ij} and d_i which minimize the following residual function:

$$\begin{aligned} \phi(c_{ij}, d_i) \equiv & \int_{-r_o}^{r_o} \int_{-r_o}^{r_o} \left[r_o^{-2} \left(1 + \frac{\xi^2}{r_o^2} + \frac{\eta^2}{r_o^2} \right)^{-3/2} \right. \\ & \left. \times \left(\frac{\partial \xi}{\partial x} \frac{\partial \eta}{\partial y} - \frac{\partial \xi}{\partial y} \frac{\partial \eta}{\partial x} \right) - \lambda^2 \right]^2 dx dy \end{aligned} \quad (2-26)$$

This residual function is obtained by considering Equation (2-10) or (2-12). Then, $\phi(c_{ij}, d_i)$ is evidently equal to zero for the exact transformation function $f(x, y)$. For computational purposes, Equation (2-26) is replaced by

$$\begin{aligned} \phi(c_{ij}, d_i) = & \sum_{x_k} \sum_{y_l} \left[r_o^{-2} \left(1 + \frac{\xi^2}{r_o^2} + \frac{\eta^2}{r_o^2} \right)^{-3/2} \right. \\ & \left. \times \left(\frac{\partial \xi}{\partial x} \frac{\partial \eta}{\partial y} - \frac{\partial \xi}{\partial y} \frac{\partial \eta}{\partial x} \right) - \lambda^2 \right]^2 \end{aligned} \quad (2-27)$$

where the points (x_k, y_l) are chosen to form a regular grid over the plane square. A computer software program for performing this minimization problem is given in Appendix E. For a second-degree approximation of the series in Equation (2-23), the following values of c_{ij} and d_i are obtained:

$$c_{00} = -2.7217 \ 05366 \ 1814$$

$$c_{10} = -5.5842 \ 16830 \ 5430$$

$$c_{01} = 2.1711 \ 17480 \ 9423$$

$$c_{20} = -3.4578 \ 62747 \ 3390$$

$$c_{11} = -6.4160 \ 15152 \ 6783$$

$$c_{02} = 1.9736 \ 26575 \ 8872$$

$$d_0 = 1.4833 \ 12929 \ 4187$$

$$d_1 = 1.1199 \ 72606 \ 9742$$

$$d_2 = 6.0515 \ 38216 \ 1464$$

The corresponding mapping function $f(x, y)$ is accurate to about five significant figures.

2.3 DERIVATION OF INVERSE MAPPING FUNCTION

Corresponding to the symmetrical direct mapping function expressed in Equation (2-14), it may be verified that the inverse mapping function is also symmetrical, i.e.,

$$x = f^*(\xi, \eta) \tag{2-28}$$

$$y = f^*(\eta, \xi)$$

As discussed in Appendix A, $f^*(\xi, \eta)$ must be expressed in the form

$$\begin{aligned}
 f^*(\xi, \eta) = & \gamma^* \xi + \frac{(1 - \gamma^*)}{r_o^2} \xi^3 \\
 & + \xi \eta^2 \left(r_o^2 - \xi^2 \right) \left[\delta^* + \delta_1^* \left(r_o^2 - \xi^2 \right) + \left(r_o^2 - \eta^2 \right) \sum_{\substack{i \geq 0 \\ j \geq 0}} c_{ij}^* \xi^{2i} \eta^{2j} \right] \\
 & + \xi^3 \left(r_o^2 - \xi^2 \right) \left[\omega^* + \left(r_o^2 - \xi^2 \right) \sum_{i \geq 0} d_i^* \xi^{2i} \right]
 \end{aligned} \tag{2-29}$$

where

$$\begin{aligned}
 \gamma^* &= \frac{1}{\gamma} \\
 \mu^* &= \frac{1}{\mu} \\
 \gamma_1^* &= \frac{1}{\gamma + r_o^4 \delta} \\
 \mu_1^* &= \frac{1}{\mu + 2r_o^4 \delta} \\
 \delta^* &= \frac{(\mu_1^* - \mu^*)}{2r_o^4} \\
 \omega^* &= \frac{1}{2r_o^4} \left(3 - 2\gamma^* - \mu^* - 2r_o^4 \delta^* \right) \\
 \delta_1^* &= \frac{1}{r_o^2} \left[\frac{(\gamma_1^* - \gamma^*)}{r_o^4} - \delta^* \right]
 \end{aligned} \tag{2-30}$$

An approximate inverse mapping function may be obtained by truncating the series expansion in Equation (2-29) at some degree, and then obtaining the coefficients c_{ij}^* and d_i^* which minimize the following residual function:

$$\begin{aligned} \phi^*(c_{ij}^*, d_i^*) \equiv & \int_{-r_0}^{r_0} \int_{-r_0}^{r_0} \left\{ \left[x - f^*(f(x, y), f(y, x)) \right]^2 \right. \\ & \left. + \left[y - f^*(f(y, x), f(x, y)) \right]^2 \right\}^{1/2} dx dy \end{aligned} \quad (2-31)$$

In obtaining this residual function, the direct mapping function $f(x, y)$ is considered, as given by Equation (2-23). Then, $\phi^*(c_{ij}^*, d_i^*)$ is evidently equal to zero for the exact inverse mapping function $f^*(\xi, \eta)$. Again, for computational purposes, Equation (2-31) is replaced by

$$\begin{aligned} \phi^*(c_{ij}^*, d_i^*) = & \sum_{x_k} \sum_{y_\ell} \left\{ \left[x - f^*(f(x, y), f(y, x)) \right]^2 \right. \\ & \left. + \left[y - f^*(f(y, x), f(x, y)) \right]^2 \right\}^{1/2} \end{aligned} \quad (2-32)$$

A computer software program for performing this minimization problem is also given in Appendix E. For a second-degree approximation of the series in Equation (2-29), the following values of c_{ij}^* and d_i^* were obtained:

$$c_{00}^* = 3.973 \quad 89249$$

$$c_{10}^* = 6.591 \quad 19476$$

$$c_{01}^* = -25.368 \quad 92536$$

$$c_{20}^* = -73.064 \quad 97000$$

$$c_{11}^* = 77.381 \ 61133$$

$$c_{02}^* = 21.685 \ 89623$$

$$d_0^* = 1.811 \ 28250$$

$$d_1^* = 37.635 \ 47857$$

$$d_2^* = 63.000 \ 23655$$

The corresponding mapping function $f^*(\xi, \eta)$ is accurate to about five significant figures.

SECTION 3 - ORGANIZATION OF DATA BASE

3.1 SUMMARY

This section mainly is concerned with the organization of the data base, whose basic structure is derived from the equal-area division of the spherical cube. It suffices, therefore, to limit most of the discussion to just one spherical square. The binary indexing scheme of the data base will be described. The reasons for adopting this indexing scheme are then discussed. This is then followed by an outline for computing the serial string index for the cell addresses.

3.2 INDEXING OF DATA BASE

The nature of the data base system adopted is extremely simple since all data are stored in a single large array. This organization is natural since:

1. The contemplated data base corresponds to a completely filled array
2. No data item has other than a positional relationship to another

Thus, all data in the data base may be accessed by directly calculated positional indices with no storage inefficiencies due to unused areas of the array.

The mapping of the data base onto storage may be accomplished in a number of ways. The classic method is mapping by columns and rows, as is done in FORTRAN array storage and as implied in the usual mathematical matrix notation. Other mapping techniques include scatter storage in which a psuedo-random, one-to-one mapping is employed as well as various consistent logical stringing techniques.

The specific scheme studied in this report is based on the binary division scheme discussed in Reference 1. This mapping starts at the level of the faces

of the spherical cube, numbering these faces 1 through 6 as in Figure 3-1. Each face is divided, to the requisite resolution level, by a two-dimensional binary grid, as shown in Figure 3-2. On each level of division, the areas are divided into quadrants, which are labeled by a 2-bit binary number. Each level of division, n , is indicated by the addition of two binary bits to the least-significant end of a $2N$ bit binary number. This binary index is the serial location of a point in the $2N$ location data array.

An address to the third level of division would appear as in Figure 3-3.

This organization will be referred to as the serial addressing scheme, and the data array as the serial data string.

3.3 REASONS FOR ADOPTING INDEXING SCHEME

In developing a method of ordering data in the data base, there are three obvious advantages to using a serial addressing scheme rather than a normal column and row addressing scheme:

1. Reduction in I/O time through maintenance of near-neighbor relationships
2. Compactness of arrays containing addresses
3. Maintenance of a consistent addressing scheme regardless of resolution level

The serial addressing scheme reduces I/O time for disk type storage devices because more near neighbors of a point are within the range which requires no arm motion for accessing. A specific example is provided in Section 3.5.

The expression of addresses as a single bit string allows storage of addresses as single machine words, whereas a two-dimensional addressing scheme would require two or three words, including one for the face number. Finally, the expandibility and generality of the serial string permits the use at any resolution

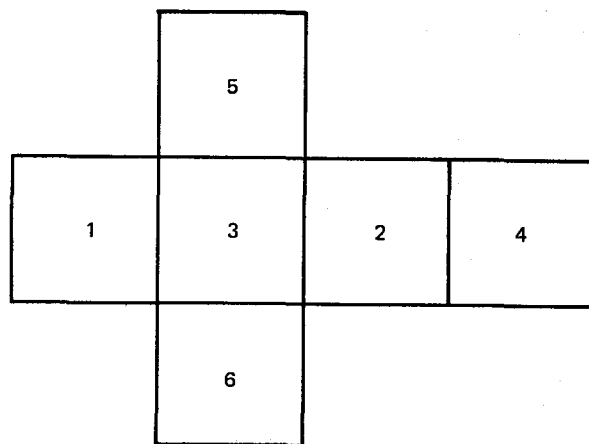


Figure 3-1. Face Numbering Scheme

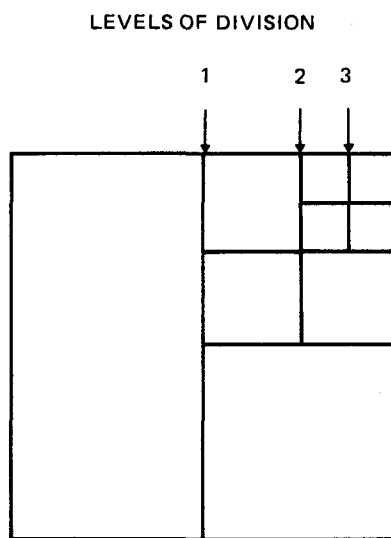


Figure 3-2. Binary Division Scheme

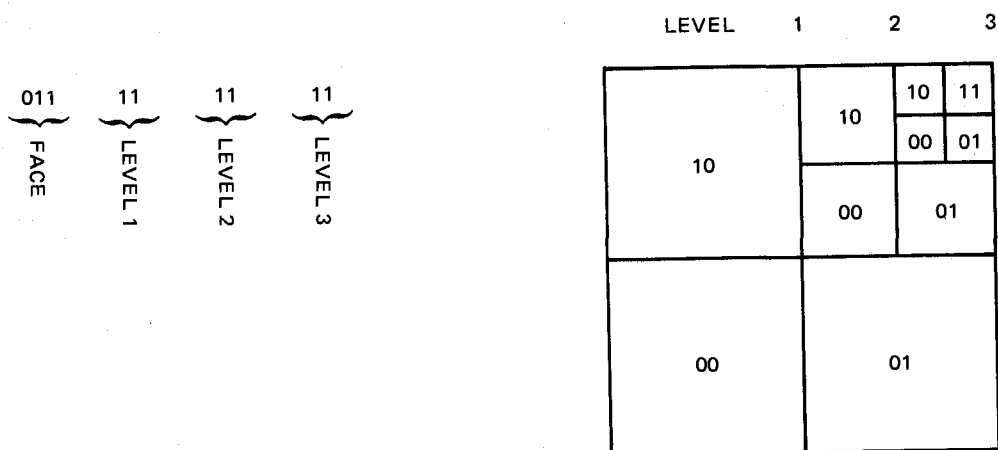


Figure 3-3. Illustrative Labeling by Binary Bits

level without regard to physical storage considerations, such as record size. Any reasonable matrix type storage scheme would require a dual (or multiple) level of addresses for record and item within record location in the serial scheme. This is accomplished simply by considering the high order m bits as the record number, and the low order $n - m$ bits as the address within record.

A major advantage discovered while studying implementation of this scheme was the extreme rapidity of index calculation. This last advantage is gained through changing the basic linking from the previously proposed pattern, shown in Figure 3-4, to that shown in Figure 3-5. This pattern retains all of the advantages of the former scheme, and also permits a simpler calculation of the serial index.

The motivation for this pattern may be best understood by considering the data base as a space filling binary tree structure in two dimensions. Figure 3-6 illustrates a simple one-dimensional tree and an associated binary numbering scheme. Figure 3-7 extends this system to two dimensions, from which it is seen that it is possible to combine the two coordinates into a one-dimensional index. This is accomplished by utilizing the even bits of a binary number to represent one coordinate and the odd bits to represent the other. Table 3-1 illustrates the values assumed by each coordinate.

For example, the addresses of the cells (1, 1) and (3, 5) will be represented in binary notation as follows:

$$(1, 1) = 01 + 10 = 11$$

$$(3, 5) = 101 + 100010 = 100111$$

The x and y coordinates may be recovered from the index by simply masking out the even or odd bits.

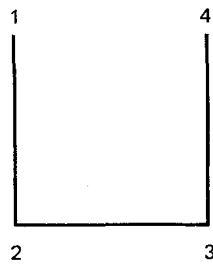


Figure 3-4. Previously Proposed Stringing Pattern

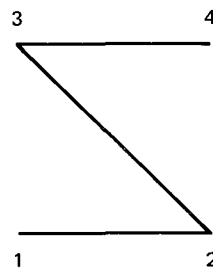


Figure 3-5. Presently Proposed Stringing Pattern

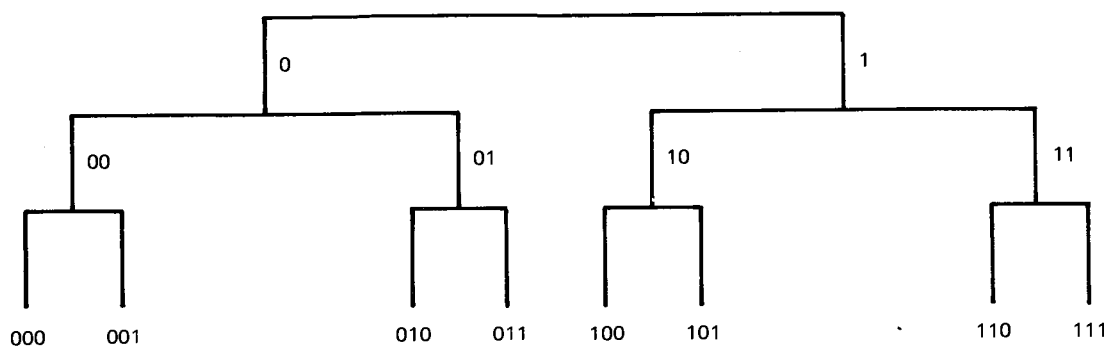


Figure 3-6. One-Dimensional Binary Tree

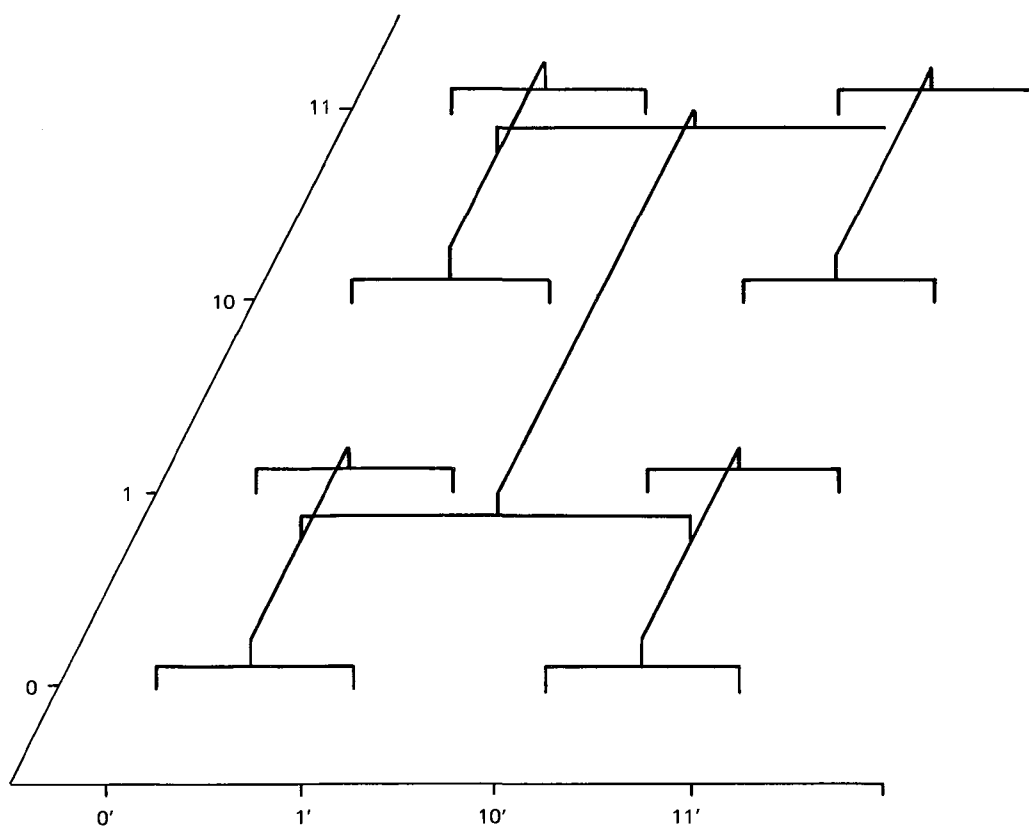


Figure 3-7. Two-Dimensional Binary Tree

Table 3-1. Binary Representation of Coordinates

DECIMAL VALUE	BINARY	X-COORDINATE (ODD)	Y-COORDINATE (EVEN)
1	1	01	10
2	10	100	1000
3	11	101	1010
4	100	10000	100000
5	101	10001	100010
6	110	10100	101000
7	111	10101	101010

In summary, the binary indexing scheme and the bit-string ordering for the first two levels of division are shown in Figure 3-8 and 3-9.

This linkage yields the desired serial string at any level. It also allows a computation of the serial address which requires only two table look-ups and an add operation.

3.4 CALCULATION OF SERIAL STRING INDEX

As mentioned in the previous section, the serial index is the composite of the x and y indices. The most rapid way of obtaining these indices is by table look-up. The construction of the y (even bit) table may be done as follows:

1. Looping over all bits in the table index
2. Examining the index bit by bit (when bit n in the index is on, set the bit $2n$ in the table entry)

The x (odd bit) table may be obtained from the even bit table by right-shifting the even bit table entries (Table 3-1).

The calculation of the serial string index may also be accomplished by the construction of a very simple hardware device. This device would consist of three registers: an x register, a y register, and a serial string or s register.

Two register-to-register instructions would provide packing from x , y to s and unpacking s to x , y . These instructions would initiate parallel transfer from the two n -bit coordinate registers to the $2n$ -bit serial register and vice versa. The interconnection is shown in Figure 3-10.

3.5 NEAR-NEIGHBOR DISTANCES IN SERIAL STRING

The serial stringing described in Section 3.3 leads to a reduction in disk I/O time because of a reduction of the number of seek operations. This happens

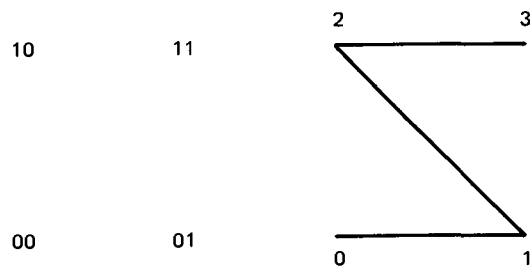


Figure 3-8. First Level of Division

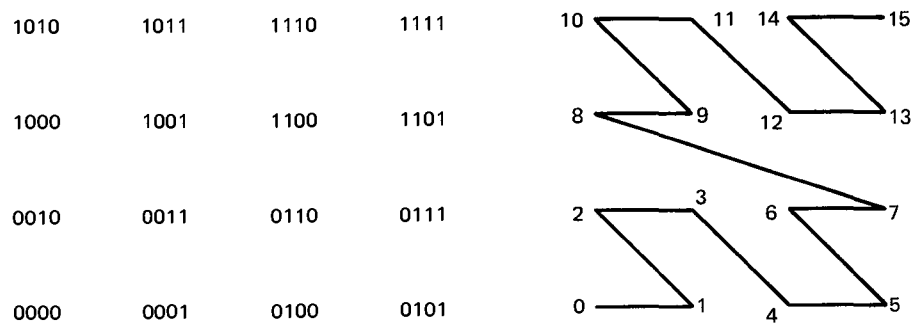


Figure 3-9. Second Level of Division

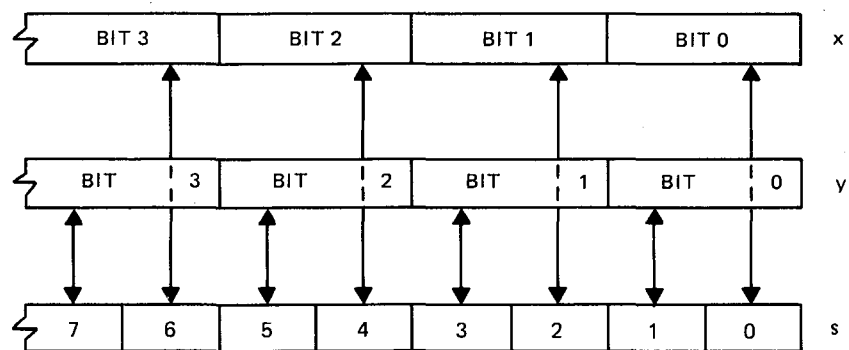


Figure 3-10. Transfer Between Registers

because the number of large gaps separating typical adjoining records is fewer for the serial string than for a matrix type storage scheme.

Figure 3-11 illustrates a resolution element and its eight adjoining spatial neighbors. The circle of radius, $r = a$, is the locus of points one resolution element away from the current point. For this situation, the probabilities of the neighbor being horizontally, vertically, or diagonally adjacent are

$$P_{\bar{h}} = 1/3$$

$$P_{\bar{v}} = 1/3$$

$$P_{\bar{d}} = 1/3$$

The individual probabilities for a specific neighbor are

$$P_h = 1/6$$

$$P_v = 1/6$$

$$P_d = 1/6$$

The matrix storage scheme (column and row storage) maintains a near-neighbor relationship only along the horizontal or vertical axis. Figure 3-12 is a graph of the probability of finding a near neighbor at a given serial separation in an $n \times n$ matrix arranged in columns and rows. The same graph for the serial string described in Section 3.3 (for a 64×64 array) appears in Figure 3-13. Depending on the definition of nearness in the serial string and the size of the array, a gain of 50 percent to 100 percent can be realized by using the serial string scheme.

The case of multi-element record stringing differs somewhat from the simple resolution elements relationship described above. In propagating the

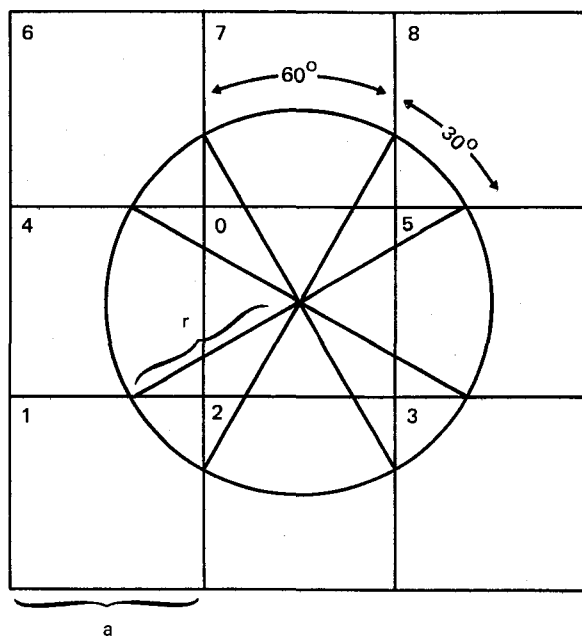


Figure 3-11. Resolution Element and Near Neighbors

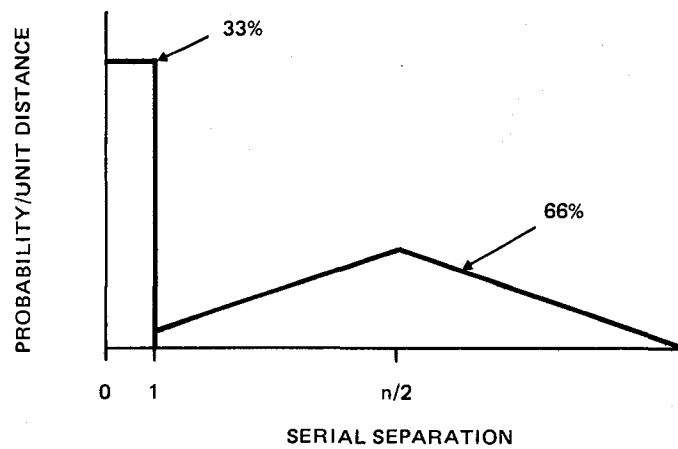


Figure 3-12. Separation of Near Neighbors in Matrix Storage

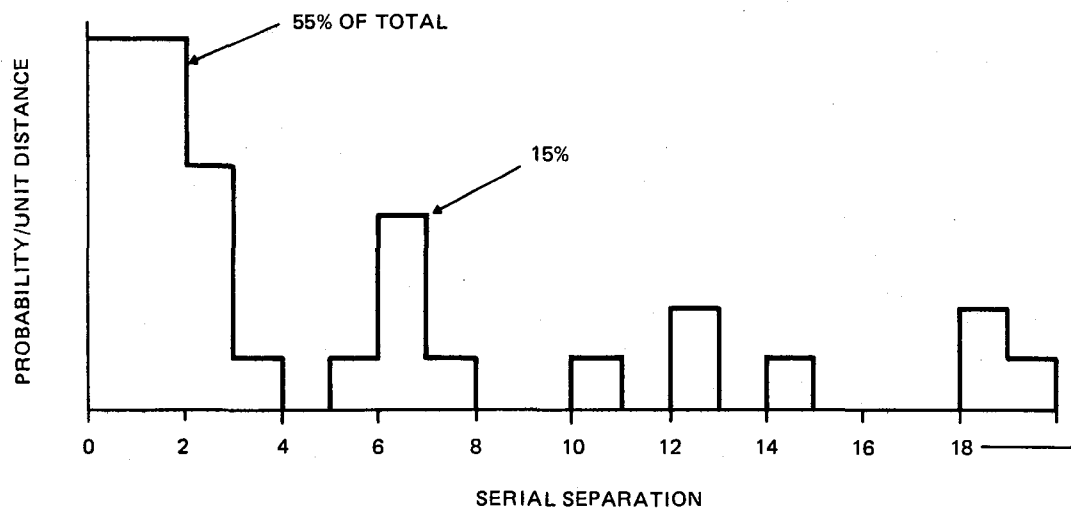


Figure 3-13. Separation of Near Neighbors in Serial String

interpolation vector, r is much less than a , and P_d becomes very small.

P_h and P_v remain equal and are approximately equal to $1/2$. Taking ± 8 records as a reasonable cylinder size, an advantage of $7/5$ is found for the serial scheme.

SECTION 4 - DATA STORAGE

4.1 SUMMARY

This section is concerned with storing data into the data base by the method of "fast-filling." The method involves the determination of benchmark points corresponding to specific scan resolution elements (pixels). The filling of neighboring data base points corresponding to neighboring pixels is then achieved by interpolation, using appropriate combinations of data base vectors and scan element vectors. This method of data base filling is possible because of the local translational invariance of the division of the spherical cube described in Section 2.

4.2 CONVERSION FROM GEOGRAPHIC COORDINATES TO DATA BASE COORDINATES

The basic objective of the fast-filling method is the insertion of data into the data base with the minimum of computation. For this purpose, it is assumed that over some small region the mapping of scan lines onto the data base yields nearly straight lines, and that the location of points along these lines can be found by interpolation. It is also assumed that there is no editing of data base information. Rather, all data are inserted into the data base as though it were initially empty.

For defining the ground location of a given pixel, the following three basic sets of information are necessary:

- Satellite orbital position
- Satellite attitude
- Time of scan

The determination of ground location (or geographic coordinates) as a function of the above parameters is described in Appendix B. Once the geographic coordinates are available, it is straightforward to obtain the corresponding set of

Cartesian coordinates (a, b, c) in the three-dimensional space. The subsequent mapping of this point into a point onto the cube representing the data base requires the following four operations:

1. Determination of the face onto which the point is to be mapped
2. Projection from the Cartesian (a, b, c) system into the curvilinear (ξ, η) system on a plane square
3. Transformation from (ξ, η) into Cartesian (x, y) coordinates on a plane square
4. Conversion from face number and (x, y) to serial location in the data base

A simple method of face determination arises naturally when a suitable relationship is chosen between the Cartesian system and the data base coordinate system. This system, illustrated in Figure 4-1, is one where each face of the data base cube is perpendicular to a major axis of the Cartesian system whose origin is at the center of the cube.

The face to which a point (a, b, c) belongs is determined by finding the component with the largest absolute value. This point is then projected into the face containing the axis corresponding to the largest component and to its sign. It should be noted at this point, however, that a point can be projected onto any of three planes, two of which are extensions of other faces. This projection is illustrated in Figure 4-2. These projections onto extended faces will have application later.

The projection from the (a, b, c) system onto the face of the cube requires the adoption of a consistent set of face coordinates. The set of face coordinate and face numbering used in Section 3 and their relation to the Cartesian system is illustrated in Figure 4-3. The projection is illustrated in Figure 4-4.

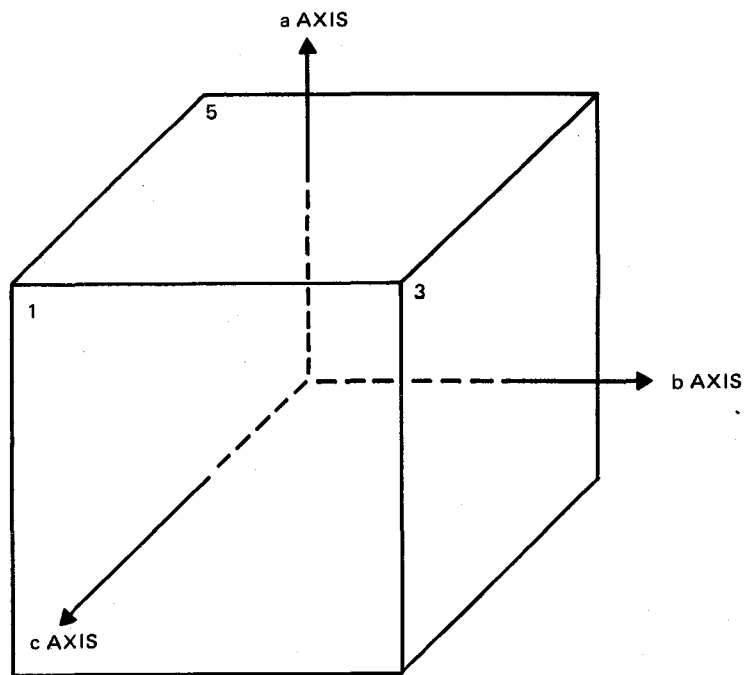


Figure 4-1. Relationship of Cartesian and Data Base Coordinate System

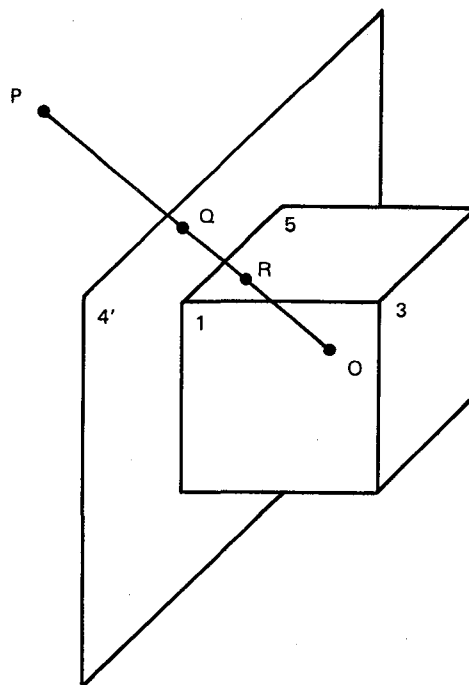


Figure 4-2. Projection of Point P Onto Face 5(R) and the Extension of Face 4(Q)

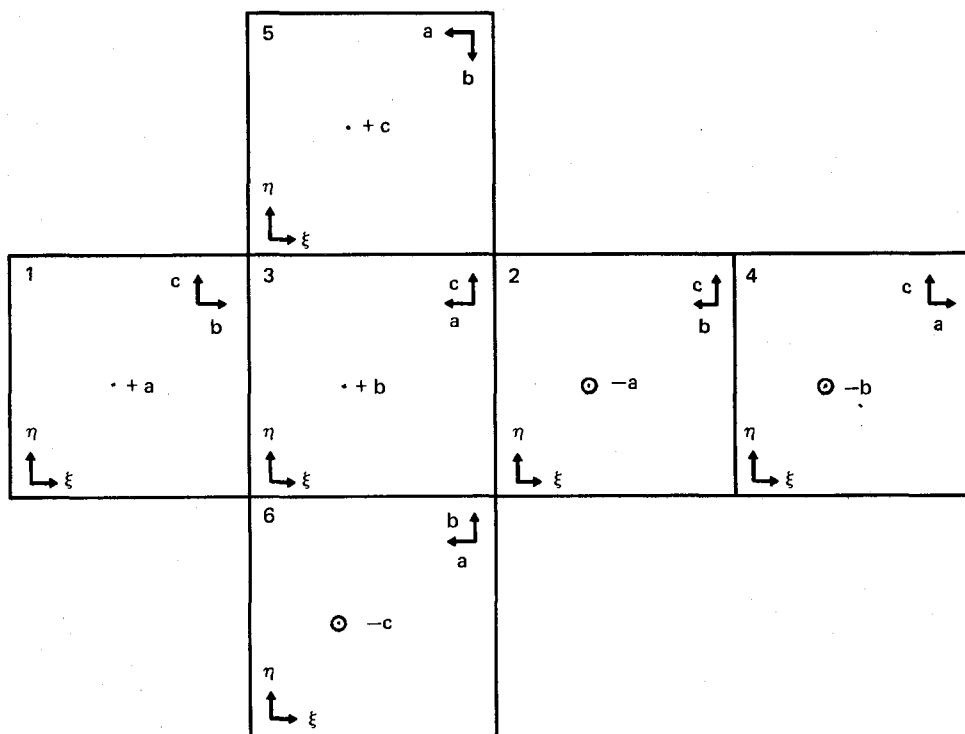


Figure 4-3. Relation of Cartesian and Face Coordinate Systems

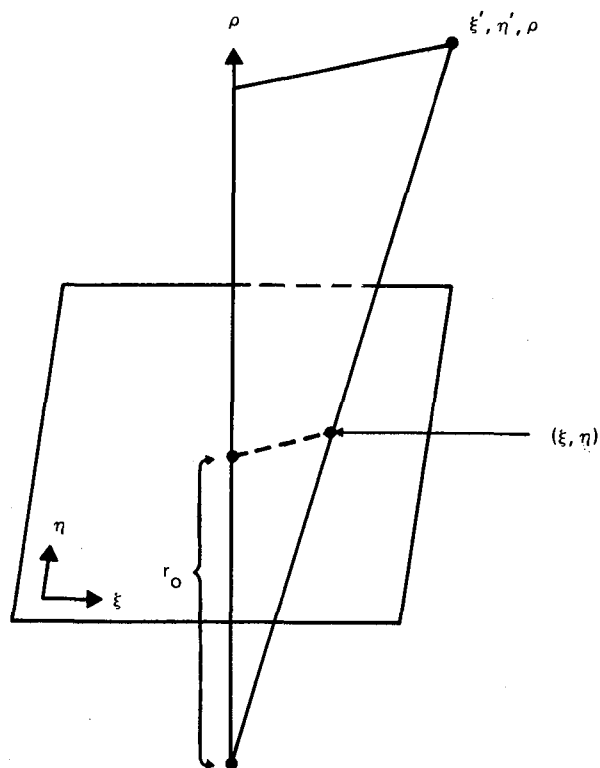


Figure 4-4. Projection of Point (ξ', η', ρ) Onto a Face

From the geometry in Figure 4-4, it is seen that the cube centered Cartesian components of the point (ξ', η', ρ) project onto the cube face (ξ, η) as follows:

$$\begin{aligned}\xi &= \xi' P \\ \eta &= \eta' P\end{aligned}\tag{4-1}$$

where $P = r_o / \rho$

From Figure 4-3, Table 4-1 is constructed illustrating relations between the (a, b, c) and (ξ', η', ρ) systems.

Table 4-1. Relations Between (a, b, c) and (ξ', η', ρ) Systems

FACE NUMBER	ξ'	η'	ρ
1	b	c	a
2	-b	c	-a
3	-a	c	b
4	a	c	-b
5	-a	-b	c
6	-a	b	-c

Using these relations, any point (a, b, c) may be mapped into an appropriate (ξ, η) system.

The transformation from the curvilinear (ξ, η) system to the rectangular data base coordinates (x, y) has been described in Section 2. The relevant equations are

$$\begin{aligned}x &= f^*(\xi, \eta) \\ y &= f^*(\eta, \xi)\end{aligned}\tag{4-2}$$

The serial data base location is obtained by table look-up as described in Section 3 or by direct calculation.

Clearly, the application of this mapping procedure to every data point would be inefficient. Consequently, it is desirable to seek methods for reducing the number of computations.

4.3 METHOD OF INTERPOLATION

The simplest method for reducing the number of computations is to utilize an interpolation method. This interpolation may be done at any one of a number of stages of the mapping from scanner coordinates to data base coordinates. The greatest reduction in computation is achieved by performing, in the data base coordinate system, a linear interpolation both along the scan line and across scan lines. Neglecting edge effects, interpolation in this frame reduces the number of transformation by a factor $N \times M$, where N is the number of pixels between calculated points, and M is the number of scan lines between calculated points. These points will be referred to as benchmarks, and the grid they form as the benchmark grid.

Interpolation (Figure 4-5) is accomplished by taking three points on the benchmark grid and constructing displacement vectors in the along-scan and across-scan directions.

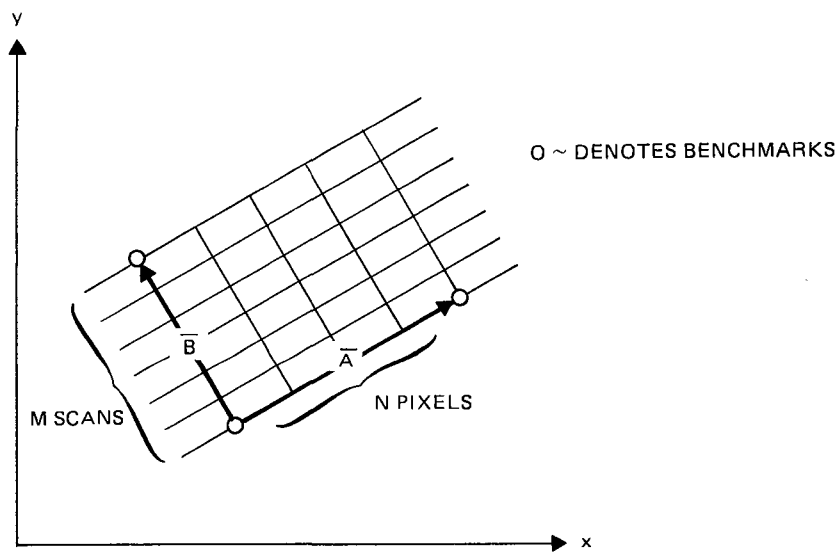


Figure 4-5. Interpolation Using Displacement Vectors

The unit displacement vectors \vec{a} , \vec{b} are obtained from

$$\begin{aligned}\vec{a} &= \vec{A}/N \\ \vec{b} &= \vec{B}/M\end{aligned}\tag{4-3}$$

Consider a pixel at point P offset by n pixels and m scan lines from the benchmark O. Then its coordinates are given by

$$\vec{OP} = n\vec{a} + m\vec{b}\tag{4-4}$$

Two factors affecting the range of interpolation are

- Curvature of scan lines in the (x, y) system
- Parallelism of scan lines over the interpolation range

The first effect was investigated by constructing great circle arcs of varying length and orientation, mapping points on these arcs into the data base, and finally comparing the mapped positions with positions obtained by interpolation between the ends of the arc. Interpolated positions were required to map onto calculated positions to an accuracy of 0.25 array element. This procedure was carried out for sets of arcs with origins at the intersections of a 5 x 5 grid covering one quadrant. Table 4-2 presents the results of this procedure.

Non-parallelism of scan lines would restrict the number of scan lines over which interpolation ranges. The primary contributor to non-parallelism would be the use of the return-scan data in an oscillating mirror scanner system. This problem does not exist for coarse resolution data since coarse resolution is averaged over a number of scans. For fine resolution, this problem can be eliminated by separating the scan lines into odd and even scans and interpolating separately.

Table 4-2. Maximum Interpolation Range as a Function of Position
in x , y Array of Dimension 4096 x 4096 (Maximum
Error 0.25 Element)

ELEMENT	CENTER					
	0	1024				2048
	0	1024	1024	512	256	64
		1024	1024	512	256	64
		512	512	256	128	32
		256	256	128	64	32
ELEMENT	2048	64	64	32	32	16
		0	1024			
				2048	VERTEX	

To maximize computational efficiency, it is desirable to interpolate over the longest range possible. Two schemes for determining this range present themselves:

- Store precalculated range in a table
- Attempt interpolation to a bench point and reduce range if interpolation is inaccurate

The precalculation method has an advantage for a system of constant resolution. The attempted interpolation method would be simpler to implement and is also applicable for variable resolution.

The largest feasible interpolation region makes a sensible logical block over which to perform computations. Such $N \times M$ rectangular blocks of data will occasionally cross a face boundary. Clearly, interpolation between points in differing (x , y) systems is meaningless. Thus a scheme for crossing these boundary regions is necessary.

A simple logical check will identify blocks which cross face boundaries. The face number bits in the four-corner benchmarks serial position can be checked against each other. If all four corners lie in one face, all points in the block must lie in that face; if any corner lies on a differing face, special measures must be taken.

Assuming that the interpolation blocks are small compared to a face, two types of face crossing may occur. These are edge crossing and vertex crossing, as illustrated in Figure 4-6.

Two types of vertex crossing may occur (Figure 4-7). Type 1 is characterized by a block having corners on three faces, and this situation may be distinguished immediately. Type 2 is characterized by a block having corners on only two faces and is difficult to distinguish from a simple edge crossing. To determine

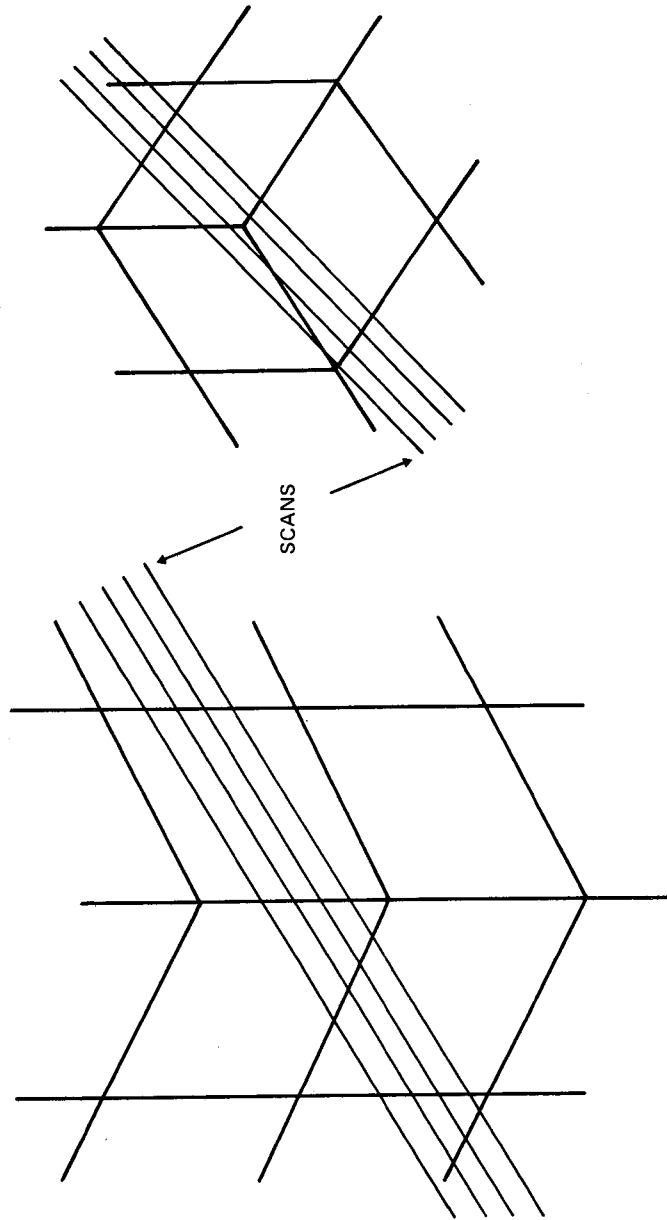


Figure 4-6. Edge Crossing and Vertex Crossing

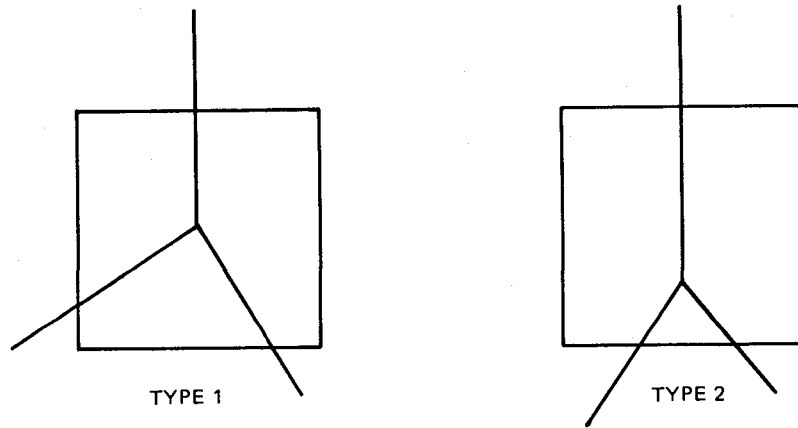


Figure 4-7. Two Types of Vertex Crossing

whether a block contains an edge crossing or a type 2 vertex crossing, the following procedure may be used:

1. Choose one face coordinate system and calculate the position of all four corners in this coordinate system. (Some of these points will lie on the extension of the face.)
2. Test this quadrilateral to see if it contains a vertex. Two tests may be used:
 - a. Construct the lines connecting the four corner benchmarks and, proceeding around the quadrilateral, determine whether or not the vertex lies to the same side of the lines connecting the benchmarks. If it does, the vertex is within the block.
 - b. A more elegant scheme is based on the fact that all of the interpolation blocks will be very nearly rhomboidal. Given this, it is then determined whether a point lies within or without the rhombus by comparing the areas of the triangles formed when the vertex point is joined to two points on the rhombus. If any of the four possible triangles has an area greater than half the rhombus area, the vertex lies outside as illustrated in Figure 4-8.

When it has been determined which and how many faces of the data base cube are involved, the interpolation method then proceeds to calculate the data base coordinate system displacement vectors for each face involved. The procedure for interpolating across edges (two face) is as follows: (1) starting at the end of a scan line, project the end point in both coordinate systems; (2) test to see which coordinate system produces a point lying in the face of that coordinate system (i.e., test x and y coordinates against the range of x and y); and (3) interpolate in that system, testing against the range of (x, y) accordingly. When a point exceeds the range of (x, y) , change systems and continue. In

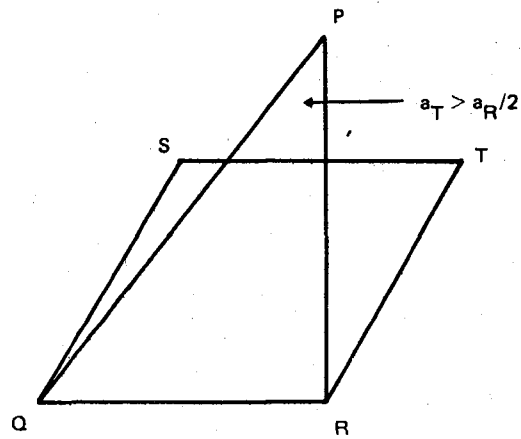


Figure 4-8. Vertex Point P Lies Outside $QRST$

the case of two faces, it is not necessary to continue testing the range since a scan line will cross only one boundary. The three-face case is similar except that, when the test fails, the other two face systems must be tested to determine which to use, and testing against the (x , y) range must continue until two-face boundaries have been crossed.

SECTION 5 - INPUT/OUTPUT MANAGEMENT

5.1 SUMMARY

In considering the design of any large-scale data base system, the efficient design of I/O management facilities is of great importance. This is especially critical in the case of a data base of this nature and magnitude. Up to this point, the data base has been considered in a general sense. This section discusses a specific data base with properties approximating an operational data base.

5.2 EXEMPLARY MODEL

Consider a data base containing whole Earth information for one spectral band consisting of one data item per pixel. As a proposed model, let each item be represented by one byte (6 or 8 bits) and let each scan line contain 1280 pixels at a resolution of 1 nautical mile, constant along the scan line.

The area of the Earth in square nautical miles is approximately

$$4\pi \times (3.48 \times 10^3)^2 = 1.52 \times 10^8$$

The nearest level of division giving coarser resolution is the 12th level

$$6 \times 4^{12} = 6 \times 4096^2 = 100663296 = 1.01 \times 10^8$$

The linear resolution of this data base is

$$\sqrt{\frac{1.52}{1.01}} = 1.22 \text{ nautical miles}$$

Therefore, at this level, 10^8 bytes of storage will be required. A convenient (but not unrealistic) model for disk type storage can be chosen to have six spindles, 256 cylinders/spindle, 16 tracks/cylinder, and 4096 bytes/track. Thus, there will be a total of $6 \times 256 \times 16 \times 4096 = 10^8$ bytes of storage. By splitting the serial data string over such a facility, it is advantageous to choose one face to correspond to one spindle, and a natural record to correspond to one track. Hence, each face would be divided into $256 \times 16 = 4096$ physical records, and each record would represent division of a face at the sixth level ($4096 = 4^6$). Because there are two bits associated with each level of division, a typical serial string address would then appear as follows:

101	111011000011	101011110011
⏟	⏟	⏟
Face Number	Physical Record Address	Address Within Record

Each physical record would thus represent an area 64 units square. This size is of the same order as the typical propagation distance for the interpolation described in Section 4. Figure 5-1 illustrates the relation of various ratios of interpolation block size to I/O record size.

In the case where the two sizes are not identical, and where the blocks and records are not perfectly aligned, a certain amount of redundant I/O transfer is inevitable. The amount of redundant transfer decreases as the ratio of interpolation to record size increases. On the other hand, the number of individual I/O operations will rise if this ratio is obtained by lowering the record size. The optimum value for this ratio will have to be determined by studying the actual machine configuration on which the data base is implemented.

For example, a 64×64 unit record has been chosen to provide reasonable savings in computation. Similarly, it is preferable to adopt the same size

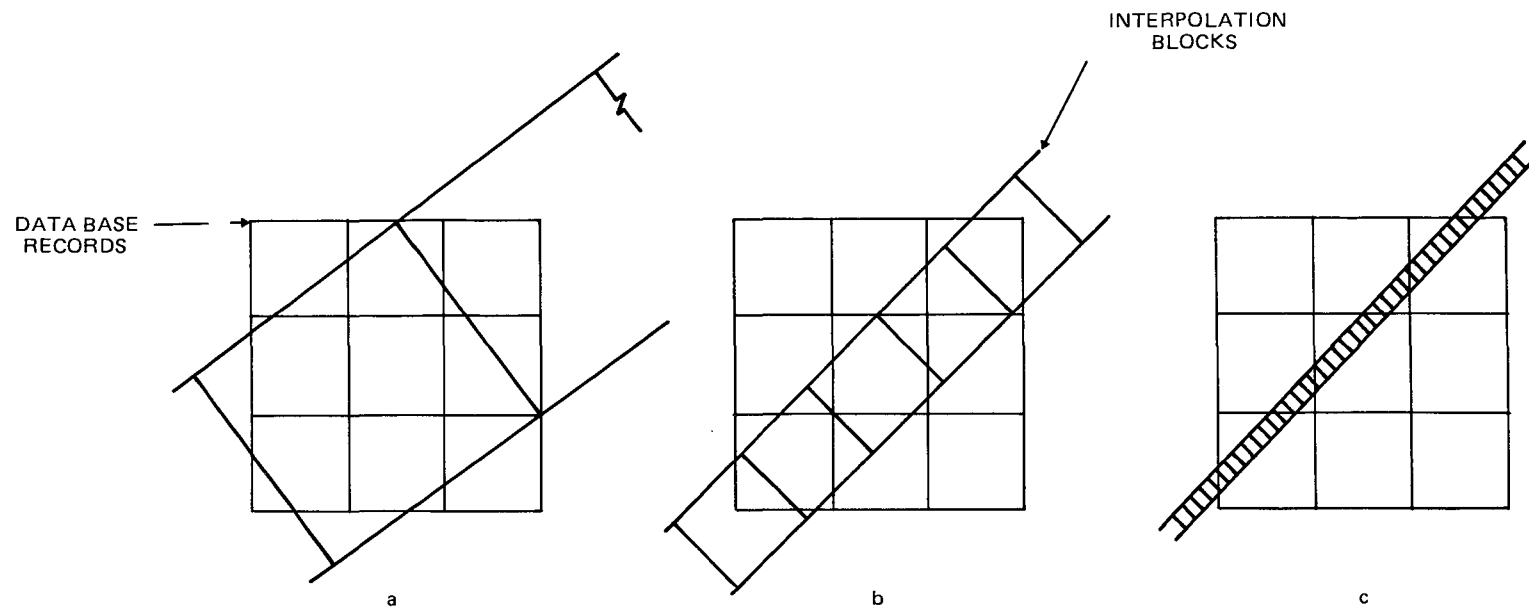


Figure 5-1. Relationship of Interpolation Blocks to I/O Records

interpolation block so that there will be $64 \times 64 = 4096$ interpolations per mapping computation. This ratio is illustrated in Figure 5-1(b). To assure complete coverage of the interpolation block, six records will be required to minimize I/O operations. Consideration must also be given to sufficient core buffer space to store all six records simultaneously, requiring 24,576 bytes of storage. Data will be queued on a first-in first-out (FIFO) basis, meaning that when a record not currently in core is required, it will replace that record which has been in core the longest. Figure 5-2 illustrates the typical result of such a scheme. Records 1 through 6 are resident in core at one time. When record 7 is required, it replaces record 1; record 8 replaces record 2; and so on.

The implementation of such a scheme is accomplished via the use of a push-down stack of fixed depth. The stack consists of a set of pointers to the initial location of a record's core location and the serial number of the record. When a record is required, the stack is searched by record number. If the record is present, the associated pointer locates the record; if the record is not present, its serial number is added to the top of the stack. The record which is pushed out of the bottom of the stack is returned to disk storage and the new record required is read into core in the newly freed locations. The pointer which was associated with the oldest record, now is associated with the new record.

The procedure for accessing the data base thus breaks down into two parts: (1) the calculation of serial addresses, and (2) the retrieval and storage of records implied by the serial addresses. As discussed previously, addresses are calculated in blocks whose size is based on the interpolation range. Taking a scan line of length 1280 pixels and the chosen 64×64 pixel interpolation block, it is required to have $64 \times 1280 = 81,920$ bytes divided into 20 64×64 pixel blocks. Looping over pixels and scan lines in these blocks, calculations will be performed for the serial address as previously discussed. Each serial

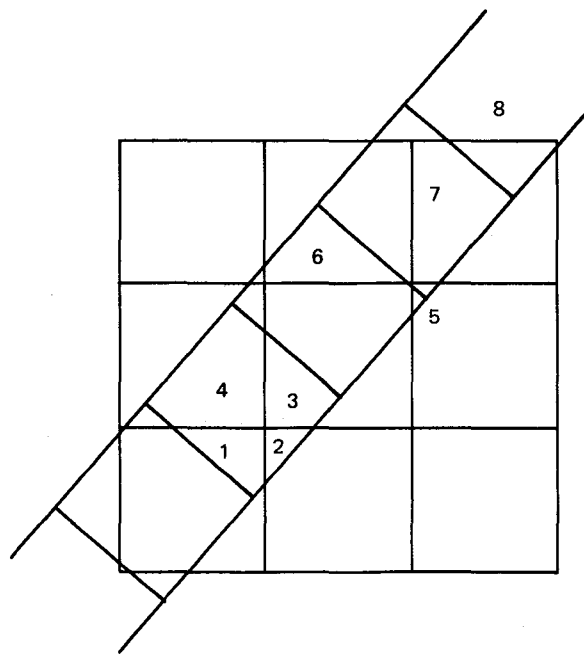


Figure 5-2. Order of First Appearance for I/O Records

address, as it is computed, is compared under a mask with the previous serial address to test for a change in physical record number. If there is no required change in record number, the data item is stored into the core location found by summing the within-record portion of the address and the base address currently in use. On the other hand, if there is a change in the record number, the new record desired is compared with the list of records in core (the stack), and an I/O operation is performed when appropriate. The base address for this new record (as stored in the stack) now becomes the active base address, and the data item is stored in the appropriate location.

The primary features of the preceding scheme are

1. I/O takes place only when a location is not available in the core buffer
2. All memory references may make use of a base address register
3. Testing for correctness of the current record requires only a simple test under mask operation

Examination of Figure 5-2 shows that record changes take place approximately once per scan line or once per 64 address computations. Thus, each interpolation block requires access to two or three records not currently in the stack (say 2.5 as a conservative estimate). The time required for a record change not necessitating an I/O operation is negligible (six comparison operations every 64 address calculations). However, the time required when I/O takes place is considerable.

To calculate the I/O time required, consider the following realistic but conservative set of specifications for a disk storage device:

- Data transfer rate: 500,000 bytes/second
- Average rotational latency: 10 msec
- Average seek time: 30 msec

At the 500K baud transfer rate, one 4096 byte record would take 8 msec. The near-neighbor relationship established by the serial addressing scheme assures that approximately 75 percent of the immediate neighbors of a record will lie on the same cylinder, thus giving an average access time of 15 msec. Using the estimate of 2.5 data base accesses per 64×64 block and the fact that each access involves one input and one output operation, it is found to require an I/O time of $5 \times (15 + 8) = 115$ msec per block or 2.3 seconds per 64 scan line input block. This yields approximately 900 I/O seconds per orbit, comfortably faster than a real-time value of 6000 seconds.

Another way of looking at this I/O requirement is that it would take approximately 2700 seconds or $3/4$ hour to fill six faces of 4096 records each. These figures are conservative and could be improved considerably by using faster hardware and by spreading adjacent records over corresponding cylinders of all available spindles. In any case, the I/O requirements are clearly well within the state of the art and would not unduly overload a large-scale, multi-purpose computer system.

5.3 HIGHER RESOLUTION DATA BASES AND USE OF SELECTED AREAS

A whole Earth data base at one mile resolution requires 10^8 bytes of storage per spectral band. This number is within the range of current disk storage devices. A higher resolution data base would, however, rapidly exceed the capacities of even the largest disk type storage devices. A data base at 0.1 mile resolution would require 10^{10} bytes, corresponding to literally hundreds of disk packs. Mass storage devices, as described in Appendix C, would allow storage of such an array.

The basic record addressing scheme discussed in Section 5.2 requires online access to a full six-faced data base. For purposes of storing high resolution data, some scheme for storing selected areas is necessary. The simplest

method of accomplishing this is by using an indirect addressing scheme. Figure 5-3 shows a face divided at the fourth level.

Blocks of records corresponding to these fourth-level areas can be stored for regions of interest. An array containing a logical flag specifying the existence of records would be stored along with a pointer indicating the real starting record number for the block. For a fourth-level division, two $16^2 = 256$ arrays will be required to store the flags and pointers.

The I/O management module in the program would first do a shift to determine the storage block number, check this against the flag array, and accordingly access the record by adding the within-block portion of the record number to the starting record number for that block.

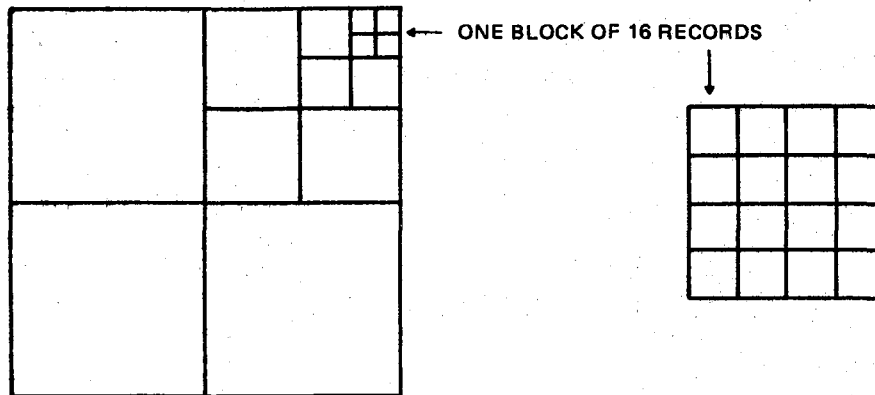


Figure 5-3. Face Divided at Fourth Level for Windowing

SECTION 6 - DATA RETRIEVAL

6.1 SUMMARY

This section is concerned with accessing data from the data base for the purposes of (1) numerical processing and (2) visual display. These are considered to be the two main needs of the contemplated user who would be interested in using the system.

6.2 DATA ACCESS FOR USER NEEDS

For the two purposes mentioned above, retrieval in physical record units would usually make sense. For most visual purposes, shape distortion would be serious only in the vertex regions where 120-degree angles map into 90-degree angles. This distortion could be minimized by using an overlay grid.

For numeric purposes, the equal-area property of the data base should make the face coordinate systems extraordinarily useful. Most applications will, however, require a conversion to a more normal two-dimensional mapping (raster) scheme. An algorithm which accomplishes this conversion is presented in the source listing attached as Appendix E.9.

For visual purposes, a useful display scheme would be to display an unfolded cube as in Figure 1-6, featuring continental outlines and a data base coordinate grid. The user could access any record or group of records by indicating the corners of the desired area with a light pen or some other device. The system would then retrieve the indicated records, convert to raster form, and display. Precalculated geographic or other grids could be overlayed on the data to provide referencing.

Alternatively, the data base system could be reconverted into a geographic grid system by reversing the mapping and interpolation procedure and applying the transformation:

$$\xi = f(x, y)$$

$$\eta = f(y, x)$$

Interpolation and I/O considerations would be similar to those described previously except that no output operations would be necessary.

A particularly rapid scheme for display would involve the use of a special piece of hardware, similar to the x, y register summing device discussed earlier. A serial address decoder accessing storage via a direct memory access (DMA) type device would allow display of a selected set of records with no central processor activity other than I/O. In a distributed system, such as that described in Appendix D, this device would be part of a stand-alone display device accessing data on a staging device.

SECTION 7 - RESULTS OF STUDY

7.1 SUMMARY

The primary result of this study is the conclusion that implementation of a Quadrilateralized Spherical Cube Data Base is feasible using current large-scale computer systems. Numerical results supporting this conclusion are presented below.

7.2 NUMERIC RESULTS OF MAPPING FUNCTION

The transformation function $f(x, y)$ described in Section 2.2 was studied intensively. A FORTRAN program was written to minimize the residual function ϕ . The function was evaluated at 36 locations on a regular grid covering one quadrant of a face. (The symmetry of Equation (2-14) permits the generalization to the other three quadrants of the face.)

Table 7-1 illustrates the very nearly equal-area nature of the projection. The table presents the ratio

$$\left[\frac{\left(\frac{\partial \xi}{\partial x} \frac{\partial \eta}{\partial y} - \frac{\partial \xi}{\partial y} \frac{\partial \eta}{\partial x} \right)}{\lambda^2 r_o^2 \left(1 + \frac{\xi^2}{r_o^2} + \frac{\eta^2}{r_o^2} \right)^{3/2}} \right]$$

which appears in Equation (2-26). In other words, it presents the transformed area at a given point normalized to the projected area at the center of a face. For an exact transformation, this ratio is identically equal to unity. The calculated root mean-square deviation over the entire face is found to be 0.000103.

The function $f^*(\xi, \eta)$ was obtained from $f(x, y)$ as indicated in Section 2.3. The procedure employed was to minimize the residual function ϕ^* calculated on the same regular grid covering one equadrant of a face.

Table 7-1. Tabulation of Direct Mapping Function Accuracy

	CENTER					
	0.0	0.2	0.4	0.6	0.8	1.0
0.0	1.0	1.0001	0.9999	0.9999	1.0001	1.0
0.2	1.0001	1.0002	1.0001	1.0001	1.0001	1.0002
0.4	0.0	1.0001	1.0	1.0001	0.9999	1.0002
0.6	0.9999	1.0001	1.0001	1.0	0.9999	1.0001
0.8	1.0001	1.0001	0.9999	0.9999	1.0001	0.9998
1.0	1.0	1.0002	1.0002	1.0001	0.9998	1.0
						VERTEX

Table 7-2 presents the results of this minimization, showing the values of

$$\sqrt{\{[x - f^*(f(x, y), f(y, x))]^2 + [y - f^*(f(y, x), f(x, y))]^2\}}$$

over the grid. For an exact inverse transformation, these values are identically equal to zero. The RMS deviation of these values is found to be 0.012.

7.3 NUMERIC RESULTS FROM TRANSFORMATION AND FAST-FILLING ALGORITHM TESTS

A FORTRAN-coded version of the $(\xi, \eta) \rightarrow (x, y)$ transformation algorithm was tested. This algorithm requires the following arithmetic operations to map one point:

Arithmetic comparisons	3
Integer multiplication	1
Integer subtraction	1
Real multiplications	51
Real divisions	5
Real additions	26
Real subtractions	2

In this form, the algorithm requires approximately 150 μ sec to execute on the IBM S/360-91 used for these tests.

The interpolation and tests used in the simple fast-filling method require 30 μ sec per point to calculate the serial address and store one point into a data base record. This time could be reduced somewhat by coding in assembler language, but is reasonably close to the irreducible minimum.

The two vital figures in this study are the 30 μ sec calculation time per data point and the average I/O time per point. Using the value of 115 msec per 64×64 block obtained in Section 5, this is also approximately 30 μ sec per

Table 7-2. Tabulation of Inverse Mapping Function Accuracy

	CENTER					
	0.0	0.2	0.4	0.6	0.8	1.0
0.0	0.0	0.003	0.007	0.020	0.008	0.0
0.2	0.003	0.008	0.009	0.019	0.016	0.027
0.4	0.007	0.009	0.016	0.011	0.015	0.005
0.6	0.020	0.019	0.011	0.013	0.015	0.025
0.8	0.008	0.016	0.015	0.015	0.008	0.018
1.0	0.0	0.027	0.005	0.025	0.018	0.0
						VERTEX

point. Overhead from other operations should not contribute significantly since all operations will be done in blocks of the order 10^3 . For a 1280 point scan line, computations and I/O times of the order of 0.02 second per scan line are expected.

For a 100-minute period satellite, the ground track speed is about 3.5 nautical miles/second. At 1 mile resolution, this means computation would be taking place at about 15 times the data rate. At 0.1 mile resolution, computation would be 1.5 times faster than real time.

The above figures are approximate and refer to execution times on the IBM S/360-91; they are conservative and could be improved upon by utilizing special hardware or by maximizing coding efficiency. They indicate that the implementation of a Quadrilateralized Spherical Cube Data Base is feasible on current generation, large-scale computers, particularly at coarser resolutions.

APPENDIX A - DETAILS OF MAPPING FUNCTION

A.1 DETAILS OF DIRECT MAPPING FUNCTION

Without any loss of generality, Equation (2-22) may be re-written as

$$\xi = f(x, y) = \gamma x + \frac{(1 - \gamma)}{r_o^2} x^3 + x \left(r_o^2 - x^2 \right) \left[y^2 g(x, y) + x^2 h(x) \right] \quad (A-1)$$

where $g(x, y)$ and $h(x)$ are even functions of their arguments. Differentiation with respect to x yields

$$\begin{aligned} \frac{\partial \xi}{\partial x} = & \gamma + \frac{3(1 - \gamma)}{r_o^2} x^2 + y^2 \left(r_o^2 - x^2 \right) g(x, y) - 2 x^2 y^2 g(x, y) \\ & + xy^2 \left(r_o^2 - x^2 \right) \frac{\partial g}{\partial x} + 3 x^2 \left(r_o^2 - x^2 \right) h(x) - 2 x^4 h(x) \\ & + x^3 \left(r_o^2 - x^2 \right) \frac{dh}{dx} \end{aligned} \quad (A-2)$$

Substitution of the condition in Equation (2-19) into the above equation yields

$$\mu = \left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=r_o \\ y=r_o}} = 3 - 2\gamma - 2 r_o^4 g(r_o, r_o) - 2 r_o^4 h(r_o) \quad (A-3)$$

For convenience, let δ and ω be defined by

$$\delta = g(r_o, r_o) \quad (A-4)$$

$$\omega = h(r_o)$$

It follows that $g(x, y)$ and $h(x)$ can be expressed as

$$g(x, y) = \delta + \left(r_o^2 - y^2\right) p(x, y) + \left(r_o^2 - x^2\right) s(x, y) \quad (A-5)$$

$$h(x) = \omega + \left(r_o^2 - x^2\right) q(x) \quad (A-6)$$

where $p(x, y)$, $q(x)$, and $s(x, y)$ are even functions of their arguments.

Moreover, from Equations (A-3) and (A-4), ω can be expressed in terms of δ by the equation

$$\omega = \frac{1}{2 r_o^4} \left(3 - 2\gamma - \mu - 2 r_o^4 \delta \right) \quad (A-7)$$

Next, at the point $(\xi = x = r_o, \eta = y = 0)$, it is noted that Equation (2-12) yields

$$\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=r_o \\ y=0}} \cdot \left. \frac{\partial \eta}{\partial y} \right|_{\substack{x=r_o \\ y=0}} - \left. \frac{\partial \xi}{\partial y} \right|_{\substack{x=r_o \\ y=0}} \cdot \left. \frac{\partial \eta}{\partial x} \right|_{\substack{x=r_o \\ y=0}} = 2 \sqrt{2} \gamma^2 \quad (A-8)$$

However, from the symmetry and boundary conditions imposed on the mapping function $f(x, y)$, it is evident from Figure 1-4 that

$$\begin{aligned} \left. \frac{\partial \xi}{\partial y} \right|_{\substack{x=r_o \\ y=0}} &= 0 \\ \left. \frac{\partial \eta}{\partial x} \right|_{\substack{x=r_o \\ y=0}} &= 0 \end{aligned} \quad (A-9)$$

Moreover, from the symmetry of Equation (2-14)

$$\left. \frac{\partial \eta}{\partial y} \right|_{\substack{x=r_o \\ y=0}} = \left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=0 \\ y=r_o}} \quad (\text{A-10})$$

Consequently, Equation (A-8) becomes

$$\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=r_o \\ y=0}} \cdot \left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=0 \\ y=r_o}} = 2\sqrt{2}\gamma^2 \quad (\text{A-11})$$

Equations (A-2), (A-5), (A-6), and (A-7) yield

$$\begin{aligned} \left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=r_o \\ y=0}} &= 3 - 2\gamma - 2r_o^4 h(r_o) \\ &= 3 - 2\gamma - 2r_o^4 \omega \\ &= \mu + 2r_o^4 \delta \end{aligned} \quad (\text{A-12})$$

$$\begin{aligned} \left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=0 \\ y=r_o}} &= \gamma + r_o^4 g(0, r_o) \\ &= \gamma + r_o^4 \left[\delta + r_o^2 s(0, r_o) \right] \end{aligned} \quad (\text{A-13})$$

Next, it is noted that the number of terms in $g(x, y)$ given by Equation (A-5) will be minimized by choosing

$$s(x, y) \equiv 0 \quad (\text{A-14})$$

This will also eliminate the terms $s(0, r)$ in Equation (A-13), which then becomes

$$\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=0 \\ y=r_o}} = \gamma + r_o^4 \delta \quad (\text{A-15})$$

Substitution of Equations (A-12) and (A-15) into Equation (A-11) yields

$$(\mu + 2 r_o^4 \delta)(\gamma + r_o^4 \delta) = 2\sqrt{2}\gamma^2 \quad (\text{A-16})$$

or, equivalently,

$$2 r_o^8 \delta^2 + (\mu + 2\gamma) r_o^4 \delta + (\mu\gamma - 2\sqrt{2}\gamma^2) = 0 \quad (\text{A-17})$$

Solution of this equation for $r_o^4 \delta$ yields

$$r_o^4 \delta = \frac{-B \pm \sqrt{B^2 - 4AC}}{2A} \quad (\text{A-18})$$

where

$$A = 2$$

$$B = (\mu + 2\gamma) > 0 \quad (A-19)$$

$$C = (\mu\gamma - 2\sqrt{2}\gamma^2) < 0$$

Consideration of Figure 1-4 reveals that $\delta > 0$. Hence, only the plus (+) sign is retained in Equation (A-17). Thus, the following expression is obtained for δ :

$$\delta = \frac{1}{4r_o^4} \left[-(\mu + 2\gamma) + \sqrt{(\mu^2 - 4\mu\gamma + 4\gamma^2 + 16\sqrt{2}\gamma^2)} \right] \quad (A-20)$$

$$= 0.79048 \ 64491 \ 208$$

The value of ω is obtained by using Equation (A-7):

$$\omega = \frac{1}{2r_o^4} (3 - 2\gamma - \mu - 2r_o^4 \delta) \quad (A-21)$$

$$= -1.2254 \ 41487 \ 984$$

Finally, in view of the above discussion, the direct mapping function $f(x, y)$ can be chosen to have the form

$$f(x, y) = \gamma x + \frac{(1 - \gamma)}{r_o^2} x^3 + xy^2 \left(r_o^2 - x^2 \right) \left[\delta + (r_o^2 - y^2) \sum_{i \geq 0} c_{ij} x^{2i} y^{2j} \right] \quad (A-22)$$

$$+ x^3 (r_o^2 - x^2) \left[\omega + (r_o^2 - x^2) \sum_{i \geq 0} d_i x^{2i} \right]$$

A.2 DETAILS OF INVERSE MAPPING FUNCTION

From Equation (2-12) and the following property of Jacobians

$$J\left(\frac{\xi, \eta}{x, y}\right) \cdot J\left(\frac{x, y}{\xi, \eta}\right) \equiv 1 \quad (\text{A-23})$$

it follows that the inverse transformation

$$\begin{aligned} x &= x(\xi, \eta) \\ y &= y(\xi, \eta) \end{aligned} \quad (\text{A-24})$$

satisfies the following equation

$$\frac{\partial x}{\partial \xi} \frac{\partial y}{\partial \eta} - \frac{\partial x}{\partial \eta} \frac{\partial y}{\partial \xi} = \frac{1}{\gamma^2 \left(1 + \frac{\xi^2}{r_o^2} + \frac{\eta^2}{r_o^2}\right)^{3/2}} \quad (\text{A-25})$$

Because the direct transformation in Equation (2-14) is symmetrical, the inverse transformation is also symmetrical, i.e.,

$$\begin{aligned} x &= f^*(\xi, \eta) \\ y &= f^*(\eta, \xi) \end{aligned} \quad (\text{A-26})$$

Proceeding as in Section 2.2, it is seen that the following four conditions are the counterparts of Equations (2-16) through (2-19)

$$f^*(0, \eta) = 0 \quad (\text{A-27})$$

$$f^*(r_o, \eta) = r_o \quad (A-28)$$

$$\left. \frac{\partial x}{\partial \xi} \right|_{\substack{\xi=0 \\ \eta=0}} = \left. \frac{\partial y}{\partial \eta} \right|_{\substack{\xi=0 \\ \eta=0}} = \frac{1}{\gamma} \equiv \gamma^* \quad (A-29)$$

$$\left. \frac{\partial x}{\partial \xi} \right|_{\substack{\xi=r_o \\ \eta=r_o}} = \left. \frac{\partial \eta}{\partial y} \right|_{\substack{\xi=r_o \\ \eta=r_o}} = \frac{1}{\mu} \equiv \mu^* \quad (A-30)$$

Thus, the first three conditions above may be incorporated into the following expansion which is the analog of Equation (A-1):

$$x = f^*(\xi, \eta) = \gamma^* \xi + \frac{(1 - \gamma^*)}{r_o^2} \xi^3 + \xi(r_o^2 - \xi^2) \left[\eta^2 g^*(\xi, \eta) + \xi^2 h^*(\xi) \right] \quad (A-31)$$

where

$$g^*(\xi, \eta) = \delta^* + (r_o^2 - \eta^2) p^*(\xi, \eta) + (r_o^2 - \xi^2) s^*(\xi, \eta) \quad (A-32)$$

$$h^*(\xi) = \omega^* + (r_o^2 - \xi^2) q^*(\xi) \quad (A-33)$$

$$\delta^* \equiv g^*(r_o, r_o)$$

$$\omega^* \equiv h^*(r_o)$$

(A-34)

$p^*(\xi, \eta)$, $q^*(\xi)$, and $s^*(\xi, \eta)$ are even functions of their arguments.

The fourth condition, i.e., Equation (A-30), yields

$$\omega^* = \frac{1}{2 r_o^4} (3 - 2\gamma^* - \mu^* - 2 r_o^4 \delta^*) \quad (\text{A-35})$$

which is the analog of Equation (A-7).

Next, by differentiating Equation (A-31) and using Equations (A-32) through (A-35), the following analogs of Equations (A-12) and (A-15) are obtained:

$$\begin{aligned} \left. \frac{\partial x}{\partial \xi} \right|_{\substack{\xi=r_o \\ \eta=0}} &= 3 - 2\gamma^* - 2 r_o^4 \omega^* \\ &= \mu^* + 2 r_o^4 \delta^* \end{aligned} \quad (\text{A-36})$$

$$\left. \frac{\partial x}{\partial \xi} \right|_{\substack{\xi=0 \\ \eta=r_o}} = \gamma^* + r_o^4 \left[\delta^* + r_o^2 s^*(0, r_o) \right] \quad (\text{A-37})$$

However, consideration of Figure 1-4 reveals that the following expressions are also valid:

$$\left. \frac{\partial x}{\partial \xi} \right|_{\substack{\xi=r_o \\ \eta=0}} = \left[\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=r_o \\ y=0}} \right]^{-1} = \frac{1}{\mu + 2 r_o^4 \delta} \equiv \mu_1^* \quad (\text{A-38})$$

$$\left. \frac{\partial x}{\partial \xi} \right|_{\substack{\xi=0 \\ \eta=r_o}} = \left[\left. \frac{\partial \xi}{\partial x} \right|_{\substack{x=0 \\ y=r_o}} \right]^{-1} = \frac{1}{\gamma + r_o^4 \delta} \equiv \gamma_1^* \quad (\text{A-39})$$

By equating the corresponding expressions above and then solving for δ^* and $s^*(0, r_o)$, it is found that

$$\delta^* = \frac{(\mu_1^* - \mu^*)}{2 r_o^4} \quad (\text{A-40})$$

$$s^*(0, r_o) = \frac{1}{2} \left[\frac{(\gamma_1^* - \gamma^*)}{r_o^4} - \delta^* \right] \quad (\text{A-41})$$

For convenience, let δ_1^* be defined by

$$\delta_1^* = s^*(0, r_o) \quad (\text{A-42})$$

Then, it follows that $s^*(\xi, \eta)$ can be expressed as

$$s^*(\xi, \eta) = \delta_1^* + \xi^2 u^*(\xi) + \left(r_o^2 - \eta^2 \right) v^*(\xi, \eta) \quad (\text{A-43})$$

where $u^*(\xi)$ and $v^*(\xi, \eta)$ are even functions of their arguments. For the purpose of expanding $x = f^*(\xi, \eta)$ and also satisfying the six conditions described by Equations (A-27) through (A-30) and (A-38) through (A-39), it may be verified that it suffices to let

$$\begin{aligned} u^*(\xi) &\equiv 0 \\ v^*(\xi, \eta) &\equiv 0 \end{aligned} \quad (\text{A-44})$$

Finally, in view of the above discussion, the inverse mapping function $f^*(\xi, \eta)$ can be chosen to have the form

$$\begin{aligned}
 f^*(\xi, \eta) = & \gamma^* \xi + \frac{(1 - \gamma^*)}{r_o^2} \xi^3 + \xi \eta^2 \left(r_o^2 - \xi^2 \right) \left[\delta^* + \delta_1^* \left(r_o^2 - \xi^2 \right) \right. \\
 & + \left(r_o^2 - \eta^2 \right) \sum_{\substack{i \geq 0 \\ j \geq 0}} c_{ij}^* \xi^{2i} \eta^{2j} \left. \right] + \xi^3 \left(r_o^2 - \xi^2 \right) \left[\omega^* \right. \\
 & \left. - \left(r_o^2 - \xi^2 \right) \sum_{i \geq 0} d_i^* \xi^{2i} \right]
 \end{aligned} \tag{A-45}$$

APPENDIX B - DEPENDENCE OF SCAN ELEMENT LOCATION ON ORBIT AND ATTITUDE OF SATELLITE

B.1 THE CASE OF ZERO PITCH, ROLL, AND YAW

Consider an Earth-centered "auxiliary" orbital coordinate system (x^A , y^A , z^A), as illustrated in Figure B-1, such that the satellite is always located on the y^A -axis and the scan angle σ is always in the (y^A , z^A)-plane. Then, the z^A -axis is always perpendicular to the plane of the orbit, and the x^A - and y^A -axes move within the orbital plane, rotating about the z^A -axis.

It is noted that the point of intersection, Q, is such that $|\mu| < \pi/2$ so that $\cos \mu$ is always given by

$$\cos \mu = \sqrt{1 - \sin^2 \mu} \quad (B-1)$$

From the sine formula for $\triangle OPQ$, it follows that

$$\frac{\sin \sigma}{R} = \frac{\sin (\pi - \sigma - \mu)}{(R + h)} \quad (B-2)$$

Using the relation

$$\sin (\pi - \sigma - \mu) = \sin (\sigma + \mu) = \sin \sigma \cos \mu + \cos \sigma \sin \mu \quad (B-3)$$

Equation (B-2) becomes

$$\frac{\sin \sigma}{R} = \frac{\sin \sigma \cos \mu + \cos \sigma \sin \mu}{(R + h)} \quad (B-4)$$

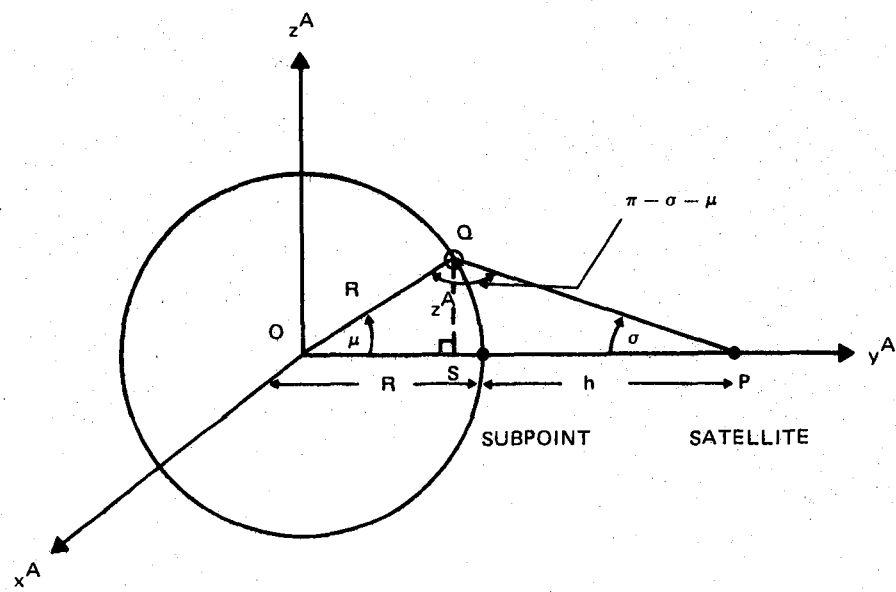


Figure B-1. Auxiliary Orbital Coordinate System

or, equivalently,

$$\cos \mu + \cot \sigma \sin \mu = \frac{(R + h)}{R} \quad (B-5)$$

Using Equation (B-1), this becomes

$$\sqrt{(1 - \sin^2 \mu)} + \cot \sigma \sin \mu = \frac{(R + h)}{R} \quad (B-6)$$

However, it is noted from $\triangle OQS$ that

$$\sin \mu = \frac{z^A}{R} \quad (B-7)$$

Hence, Equation (B-6) becomes

$$\sqrt{\left(1 - \frac{z^A^2}{R^2}\right)} = \frac{(R + h)}{R} - \cot \sigma \frac{z^A}{R} \quad (B-8)$$

or, on squaring,

$$1 - \frac{z^A^2}{R^2} = \frac{(R + h)^2}{R^2} - 2 \frac{(R + h)}{R} \cot \sigma \frac{z^A}{R} + \cot^2 \sigma \frac{z^A^2}{R^2} \quad (B-9)$$

or

$$(1 + \cot^2 \sigma) \frac{z^A^2}{R^2} - \left[2 \frac{(R + h)}{R} \cot \sigma \right] \frac{z^A}{R} + \left[\frac{(R + h)^2}{R^2} - 1 \right] = 0 \quad (B-10)$$

Solution of this equation yields

$$\frac{z^A}{R} = \frac{-B \pm \sqrt{B^2 - 4AC}}{2A} \quad (B-11)$$

where

$$\begin{aligned} A &= 1 + \cot^2 \sigma = \csc^2 \sigma \\ B &= -2 \frac{(R+h)}{R} \cot \sigma \\ C &= \frac{(R+h)^2}{R^2} - 1 \end{aligned} \quad (B-12)$$

Since the point of intersection, Q, is on the closer side to P, its z^A -coordinate is given by Equation (B-11) in which only the minus (-) sign is retained. Thus, Equation (B-11) becomes

$$\frac{z^A}{R} = \frac{(R+h)}{R} \sin \sigma \cos \sigma - \sin^2 \sigma \sqrt{\left[\csc^2 \sigma - \frac{(R+h)^2}{R^2} \right]} \quad (B-13)$$

Also, from Figure B-1 it is noted that

$$y^A = R \cos \mu = \sqrt{R^2 - z^A{}^2} \quad (B-14)$$

and

$$x^A = 0 \quad (B-15)$$

Next, consider the Earth-centered inertial coordinate system (x^I, y^I, z^I) , as shown in Figure B-2.

Then, it is well-known that the Euler angles ϕ , θ , and ψ are given by

$$\phi = \Omega \quad (B-16)$$

$$\theta = i \quad (B-17)$$

$$\psi = \omega + v - \pi/2 \quad (B-18)$$

where i = inclination of satellite orbit

Ω = longitude of ascending node

ω = argument of perigee

v = true anomaly

The coordinates of point Q are denoted by (x^I, y^I, z^I) in the two coordinate systems. For convenience, let

$$\vec{r}^I \equiv (x^I, y^I, z^I) \quad (B-19)$$

$$\vec{r}^A \equiv (x^A, y^A, z^A)$$

Then, the vectors \vec{r}^I and \vec{r}^A are related by

$$\vec{r}^I = A^{-1} \vec{r}^A \quad (B-20)$$

where A^{-1} is the matrix given by Equation (4-47) of Reference 2:

$$A^{-1} = \tilde{A} = \begin{pmatrix} \cos \psi \cos \phi - \cos \theta \sin \phi \sin \psi & -\sin \psi \cos \phi - \cos \theta \sin \phi \cos \psi & \sin \theta \sin \phi \\ \cos \psi \sin \phi + \cos \theta \cos \phi \sin \psi & -\sin \psi \sin \phi + \cos \theta \cos \phi \cos \psi & -\sin \theta \cos \phi \\ \sin \theta \sin \psi & \sin \theta \cos \psi & \cos \theta \end{pmatrix} \quad (B-21)$$

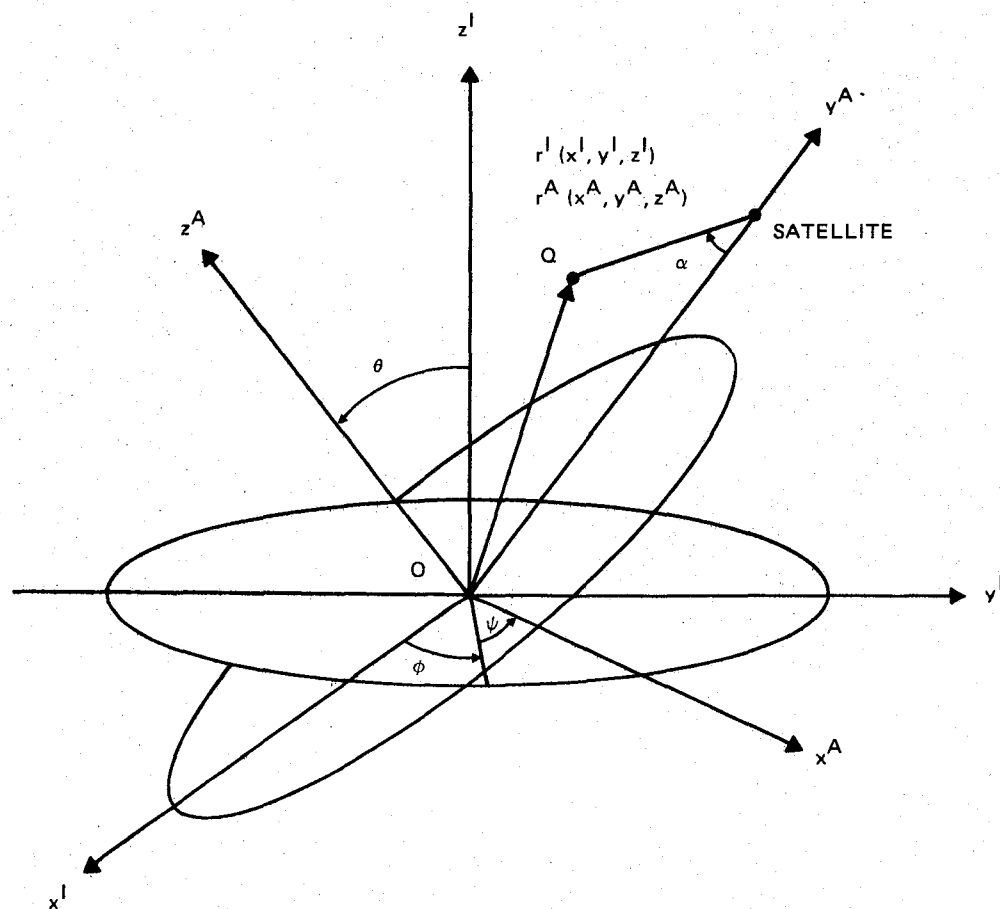


Figure B-2. Inertial Coordinate System

Hence, from Equations (B-15), (B-20), and (B-21), it follows that

$$x^I = (-\sin \psi \cos \phi - \cos \theta \sin \phi \cos \psi) y^A + (\sin \theta \sin \phi) z^A \quad (B-22)$$

$$y^I = (-\sin \psi \sin \phi + \cos \theta \cos \phi \cos \psi) y^A + (-\sin \theta \cos \phi) z^A \quad (B-23)$$

$$z^I = (\sin \theta \cos \psi) y^A + (\cos \theta) z^A \quad (B-24)$$

where y^A , z^A , ϕ , θ , and ψ are given by Equations (B-14), (B-13), (B-16), (B-17), and (B-18), respectively. Hence, the coordinates (x^I, y^I, z^I) of the point Q are obtained.

Finally, consider the uniformly, Earth-centered rotating coordinate system (x^R, y^R, z^R) as shown in Figure B-3.

It is easily shown that

$$x^R = x^I \cos \bar{\omega}t + y^I \sin \bar{\omega}t \quad (B-25)$$

$$y^R = -x^I \sin \bar{\omega}t + y^I \cos \bar{\omega}t \quad (B-26)$$

$$z^R = z^I \quad (B-27)$$

in which $t = 0$ when the two coordinate systems coincide. Thus, the coordinates of a scan element on a rotating Earth are obtained in terms of the satellite orbital position, satellite attitude, and scan angle.

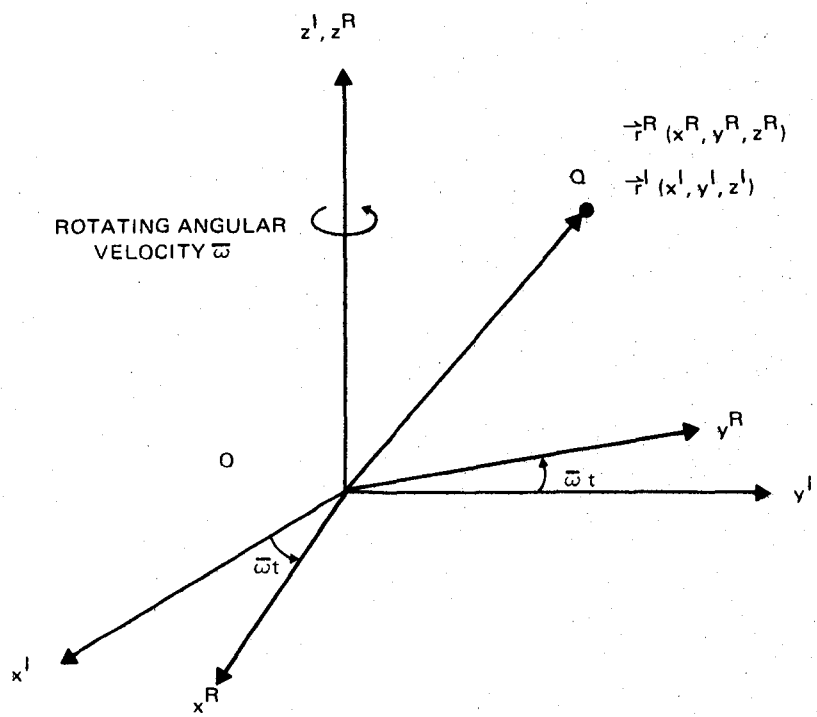


Figure B-3. Uniformly Rotating Coordinate System

B.2 THE CASE OF GENERAL PITCH, ROLL, AND YAW

Let (x^A, y^A, z^A) , (x^I, y^I, z^I) , and (x^R, y^R, z^R) , respectively denote the "auxiliary" frame, the Earth-centered inertial frame, and the Earth-centered rotating frame of reference as defined previously.

Consider an Earth-centered orbital coordinate system (x^O, y^O, z^O) defined by the unit vectors

$$\begin{aligned}\hat{x}^O &= -\hat{x}^A \\ \hat{y}^O &= -\hat{z}^A \\ \hat{z}^O &= -\hat{y}^A\end{aligned}\tag{B-28}$$

Figure B-4 illustrates the orientation of the orbital coordinate system with respect to the "auxiliary" orbital coordinate system.

Let

$$\begin{aligned}\vec{r}^A &\equiv (x^A, y^A, z^A) \\ \vec{r}^O &\equiv (x^O, y^O, z^O)\end{aligned}\tag{B-29}$$

Hence, from Figure B-4, it is seen that

$$\begin{bmatrix} x^A \\ y^A \\ z^A \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & -1 & 0 \end{bmatrix} \begin{bmatrix} x^O \\ y^O \\ z^O \end{bmatrix}\tag{B-30}$$

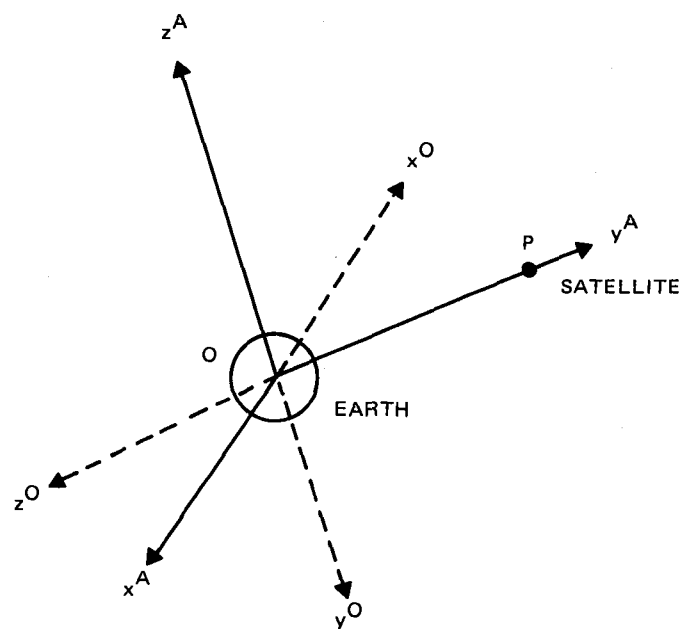


Figure B-4. Orbital Coordinate System

Therefore, the transformation

$$\vec{r}^A = B \vec{r}^O \quad (B-31)$$

has the matrix B given by

$$B = \begin{bmatrix} -1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & -1 & 0 \end{bmatrix} \quad (B-32)$$

It is noted that the satellite pitch, roll, and yaw axes are obtained by a parallel translation of the (x^O, y^O, z^O) coordinate system from O to P.

Next, consider a body-fixed coordinate system (x^B, y^B, z^B) on the satellite. Let α , β , and γ respectively denote the roll, pitch, and yaw angles which transform a vector from the orbital to the body-fixed frame. That is, if

$$\begin{aligned} \vec{r}^O &\equiv (x^O, y^O, z^O) \\ \vec{r}^B &\equiv (x^B, y^B, z^B) \end{aligned} \quad (B-33)$$

then

$$\vec{r}^B = C \vec{r}^O \quad (B-34)$$

where

$$C = \begin{bmatrix} \cos \beta \cos \gamma & \cos \alpha \sin \gamma & -\sin \beta \cos \gamma \\ + \sin \beta \sin \alpha \sin \gamma & & + \cos \beta \sin \alpha \sin \gamma \\ -\cos \beta \sin \gamma & \cos \alpha \cos \gamma & \sin \beta \sin \gamma \\ + \sin \beta \sin \alpha \cos \gamma & & + \cos \beta \sin \alpha \cos \gamma \\ \sin \beta \cos \alpha & -\sin \alpha & \cos \beta \cos \alpha \end{bmatrix} \quad (B-35)$$

Since C is an orthogonal matrix,

$$C^{-1} = C^T \quad (B-36)$$

Hence, from Equation (B-35), the following matrix is obtained for C^{-1} :

$$C^{-1} = \begin{bmatrix} C_{\beta} C_{\gamma} & -C_{\beta} S_{\gamma} & S_{\beta} C_{\alpha} \\ + S_{\beta} S_{\alpha} S_{\gamma} & + S_{\beta} S_{\alpha} C_{\gamma} & \\ C_{\alpha} S_{\gamma} & C_{\alpha} C_{\gamma} & -S_{\alpha} \\ -S_{\beta} C_{\gamma} & S_{\beta} S_{\gamma} & C_{\beta} C_{\alpha} \\ + C_{\beta} S_{\alpha} S_{\gamma} & + C_{\beta} S_{\alpha} C_{\gamma} & \end{bmatrix} \quad (B-37)$$

where the abbreviation S_{α} and C_{α} are used to denote $\sin \alpha$ and $\cos \alpha$, respectively.

Let \hat{n} denote the unit vector along the scan ray which is assumed to be in the (y^B, z^B) -plane. The scan angle, σ , is defined as in Figure B-5.

Then, in the body-fixed system, the scan ray unit vector is given by

$$\hat{n} = \hat{n}^B = -\sin \sigma \hat{y}^B + \cos \sigma \hat{z}^B \quad (B-38)$$

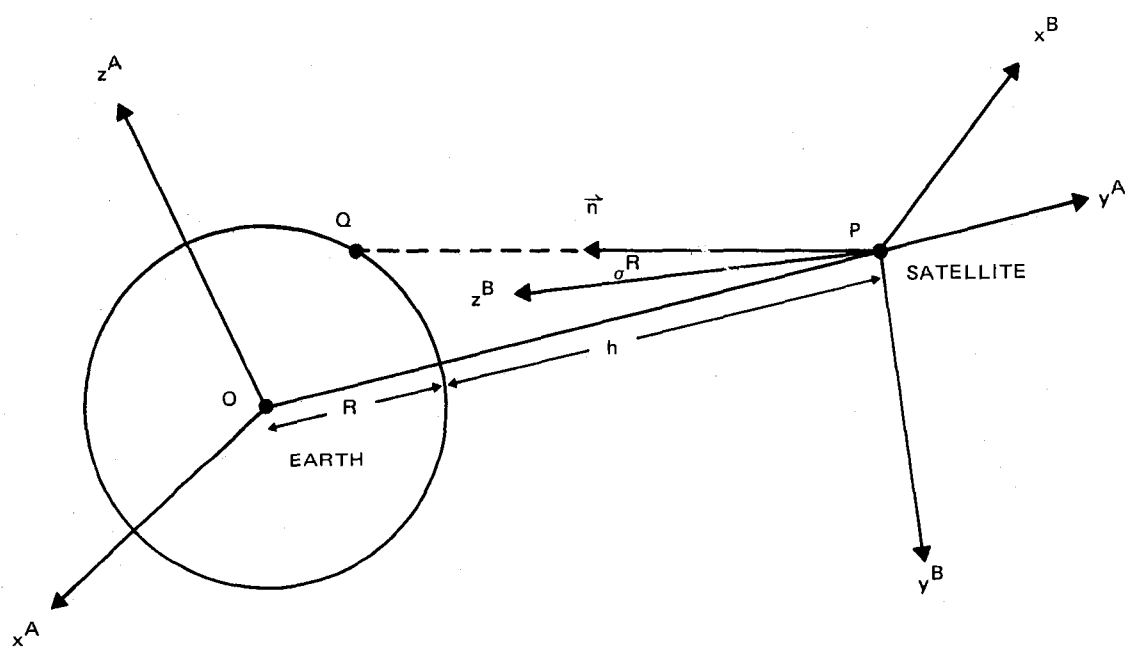


Figure B-5. Satellite Scanning Earth

In general, if the scan ray is not in the (y^B, z^B) -plane, then \hat{n}^B is given by

$$\hat{n} = \hat{n}^B = \cos \sigma_x \hat{x}^B + \cos \sigma_y \hat{y}^B + \cos \sigma_z \hat{z}^B \quad (B-39)$$

where σ_x , σ_y , and σ_z are the angles between \hat{n} and the respective body-fixed coordinate axes.

It follows from Equations (B-31) and (B-34), that in the orbital and the auxiliary orbital systems, the scan ray unit vector is given by

$$\hat{n}^O = C^{-1} \hat{n}^B \quad (B-40)$$

$$\hat{n}^A = B \hat{n}^O \quad (B-41)$$

so that

$$\hat{n}^A = B C^{-1} \hat{n}^B \quad (B-42)$$

From Equations (B-32), (B-37), and (B-38), it follows that

$$B C^{-1} = \begin{bmatrix} -C_\beta C_\gamma & C_\beta S_\gamma & -S_\beta C_\alpha \\ -S_\beta S_\alpha S_\gamma & -S_\beta S_\alpha C_\gamma & \\ S_\beta C_\gamma & -S_\beta S_\gamma & -C_\beta C_\alpha \\ -C_\beta S_\alpha S_\gamma & -C_\beta S_\alpha C_\gamma & \\ -C_\alpha S_\gamma & -C_\alpha C_\gamma & S_\alpha \end{bmatrix} \quad (B-43)$$

$${}_{BC}^{-1} \hat{n}^B = \begin{bmatrix} \{(C_\beta S_\gamma - S_\beta S_\alpha C_\gamma)(-S_\sigma) + (-S_\beta C_\alpha)(C_\sigma)\} \\ \{(-S_\beta S_\gamma - C_\beta S_\alpha C_\gamma)(-S_\sigma) + (-C_\beta C_\alpha)(C_\sigma)\} \\ \{(-C_\alpha C_\gamma)(-S_\sigma) + (S_\alpha)(C_\sigma)\} \end{bmatrix} \quad (B-44)$$

Hence, if we denote \hat{n}^A by

$$\hat{n}^A = n_x^A \hat{x}^A + n_y^A \hat{y}^A + n_z^A \hat{z}^A \quad (B-45)$$

it follows from Equations (B-31), (B-33), and (B-34) that

$$\begin{aligned} n_x^A &= (C_\beta S_\gamma - S_\beta S_\alpha C_\gamma)(-S_\sigma) + (-S_\beta C_\alpha)(C_\sigma) \\ n_y^A &= (-S_\beta S_\gamma - C_\beta S_\alpha C_\gamma)(-S_\sigma) + (-C_\beta C_\alpha)(C_\sigma) \\ n_z^A &= (-C_\alpha C_\gamma)(-S_\sigma) + (S_\alpha)(C_\sigma) \end{aligned} \quad (B-46)$$

It is obvious from Figure B-5 that by definition

$$n_y^A < 0 \quad (B-47)$$

Next, let (x^A, y^A, z^A) denote the coordinates of the point Q in the auxiliary orbital system. It is noted that the coordinates of P are $(0, R + h, 0)$.

Hence, it follows that the following ratios are equal

$$\frac{x^A}{n_x^A} = \frac{y^A - (R + h)}{n_y^A} = \frac{z^A}{n_z^A} \quad (B-48)$$

which comprise a system of two independent equations and three unknowns. The third equation is obtained by noting that the point Q lies on the sphere

$$x^2 + y^2 + z^2 = R^2 \quad (\text{B-49})$$

Hence, we obtain

$$x = \frac{n_x}{n_z} z \quad (\text{B-50})$$

$$y = \frac{n_y}{n_z} z + (R + h) \quad (\text{B-51})$$

$$\left(\frac{n_x}{n_z} z \right)^2 + \left[\frac{n_y}{n_z} z + (R + h) \right]^2 + z^2 = R^2$$

or, equivalently,

$$\left[\left(\frac{n_x}{n_z} \right)^2 + \left(\frac{n_y}{n_z} \right)^2 + 1 \right] \frac{z^2}{R^2} + \left[2 \frac{(R + h)}{R} \frac{n_y}{n_z} \right] \frac{z}{R} + \left[\frac{(R + h)^2}{R^2} - 1 \right] = 0 \quad (\text{B-52})$$

It is easily verified that Equation (B-52) reduces to Equation (B-7) for the case of zero pitch, roll, and yaw. Solution of Equation (B-52) yields

$$\frac{z^A}{R} = \frac{-B \pm \sqrt{(B^2 - 4AC)}}{2A} \quad (B-53)$$

$$\begin{aligned} A &= \left[\left(\frac{n_x^A}{n_z^A} \right)^2 + \left(\frac{n_y^A}{n_z^A} \right)^2 + 1 \right] \\ B &= \left[2 \frac{(R+h)}{R} \frac{n_y^A}{n_z^A} \right] \\ C &= \left[\frac{(R+h)^2}{R^2} - 1 \right] \end{aligned} \quad (B-54)$$

Since the point of intersection Q is on the closer side to P , its z^A -coordinate is given by Equation (B-53) in which only the minus (-) sign is retained. Equations (B-50) and (B-41) are then used to yield x^A and y^A .

The rest of the analysis is precisely the same as that in Section B.1 commencing with Figure B-2. Thus, the coordinates (x^I, y^I, z^I) of Q in the inertial system and (x^R, y^R, z^R) in the rotating system are readily obtained by the use of Equations (B-22) through (B-24) and (B-25) through (B-27).

APPENDIX C - USE OF MASS STORAGE DEVICES AND THREE-DIMENSIONAL ARRAYS

The discussion of data bases in this report has assumed that only current data would be maintained in direct-access storage. A new class of storage devices, rapid mass stores, are now becoming available. These devices open up the possibility for on-line access to noncurrent data.

These devices are characterized by the ability to store on-line up to trillions (10^{12}) of bits of information, and to transfer large blocks of data at high rates exceeding 10^6 bits/seconds. A wide variety of mechanical and electro/optical devices with these characteristics is presently coming onto the market. These devices offer either write-once/multiple-read or multiple-write and read capabilities.

A write-once system would be suitable for archiving meteorological data bases for later reference, and for processing of temporal variations. Data can be transferred to the write-once device in the case of data bases with a random access device. There are four ways of archiving the data:

1. Storing raw data for later insertion into data base format
2. Storing a snap dump of the data base on completion of a satellite orbit
3. Storing a snap dump on a sparse schedule
4. Storing data in a three-dimensional data base (including a temporal coordinate)

This last method may have excellent long-range utility in that data would be blocked together in the temporal as well as spatial sense. This permits rapid access to temporally varying data in small spatial regions without long-range searches in the mass store. This is important since all mass storage devices utilize some sort of mechanical transport for units of the storage medium.

A three-dimensional data base can be constructed by extending the serial stringing scheme to 3 bits per level, utilizing 1 bit for each coordinate. A non-cubic configuration (with fewer temporal than spatial intervals) can be achieved by adding the third bit only to N levels of division, the number of temporal intervals being 2^N . The natural temporal unit would be one orbit which is approximately 100 minutes. The third bit could be added either at the highest or lowest level, depending on the application, for efficient access to areas selected by temporal or spatial order.

A device with 10^{12} bits would have the capacity for storage of more than 100 complete 10^8 byte data bases, and additional intervals for usage on selected spatial areas.

One mass storage device familiar to CSC personnel is the UNICON device used in the ILLIAC IV system. This device gives on-line access to 2.9×10^{12} bits. The storage medium is mylar strips which are written by burning areas with a focused laser beam. This device thus belongs to the write-once class.

Mechanically, the UNICON resembles the IBM 2301 Data Cell device, utilizing a rotating read/write drum on which the storage strip is positioned. Automatic mechanical pickers give on-line access to 1000 storage strips, each containing 2.9×10^9 bits of data. The data are spread over approximately 10^4 tracks/strip with a density of about 2.5×10^5 bits/track. Data can be transferred in 10^6 -bit blocks at a rate of 4×10^6 bits/second. The interblock access time is 200 msec.

The general I/O management scheme described in Section 5 would still apply to such a device but data could be transferred in much longer records.

APPENDIX D - USE OF DISTRIBUTED PROCESSING

Implicit in Section 6 was the idea that the data base system would be implemented on a classic large-scale computer system. Substantial savings in central processor usage and greater flexibility could be obtained by distributing a number of system functions into various subsidiary devices.

A straight large-scale computer implementation would appear as shown in Figure D-1.

A simple improvement would be to place all I/O management under the control of a minicomputer which would handle all data base accesses and transfer data to the CPU via a DMA, extended core, or a staging drum as illustrated in Figure D-2.

A further elaboration would involve more elaborate minicomputer systems which would handle data input and user interaction functions. Figure D-3 shows an arrangement where a system of minicomputers relieves the CPU of all operations except calculations based on data transmitted from the data base. In such a system, either the CPU or the control minicomputer could control the system. Functions indicated as being performed on one minicomputer (such as input processing and mapping to the data base system) could actually be spread among a number of processors.

In the input processor area, orbit determination and attitude determination functions could take place in parallel in two or more units. In the mapping process, the following areas are amenable to parallel calculation:

- Mapping the ξ , η systems to x , y may be done in parallel
 $\xi \rightarrow x$ and $\eta \rightarrow y$
- Any number of interpolation blocks or scan lines could be processed in parallel if serial coordinates were outputted as strings to a separate I/O processor

- I/O processing for any number of spectral bands could be carried on in parallel

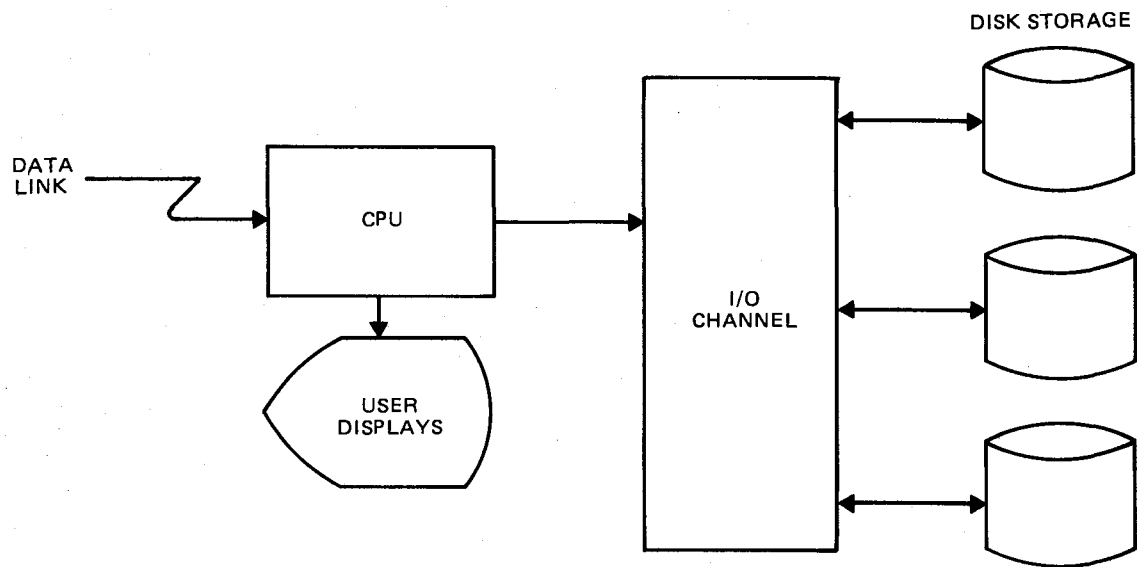


Figure D-1. Straight Large-Scale Computer Implementation

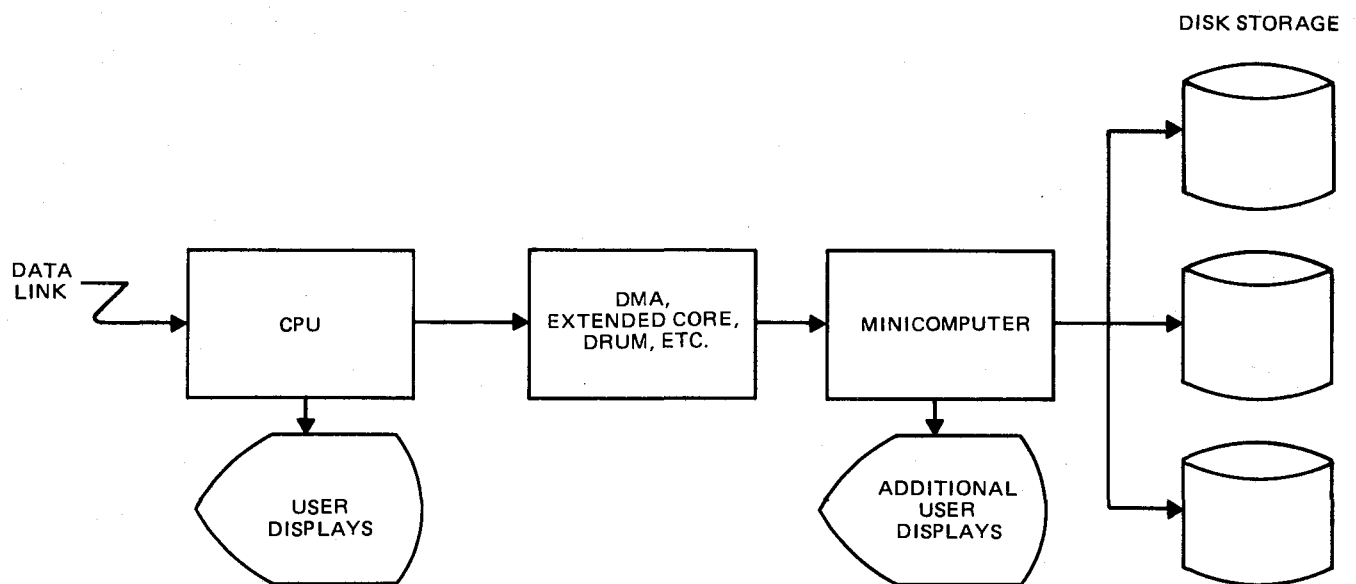


Figure D-2. Large-Scale Computer Implementation With I/O Management Under Minicomputer Control

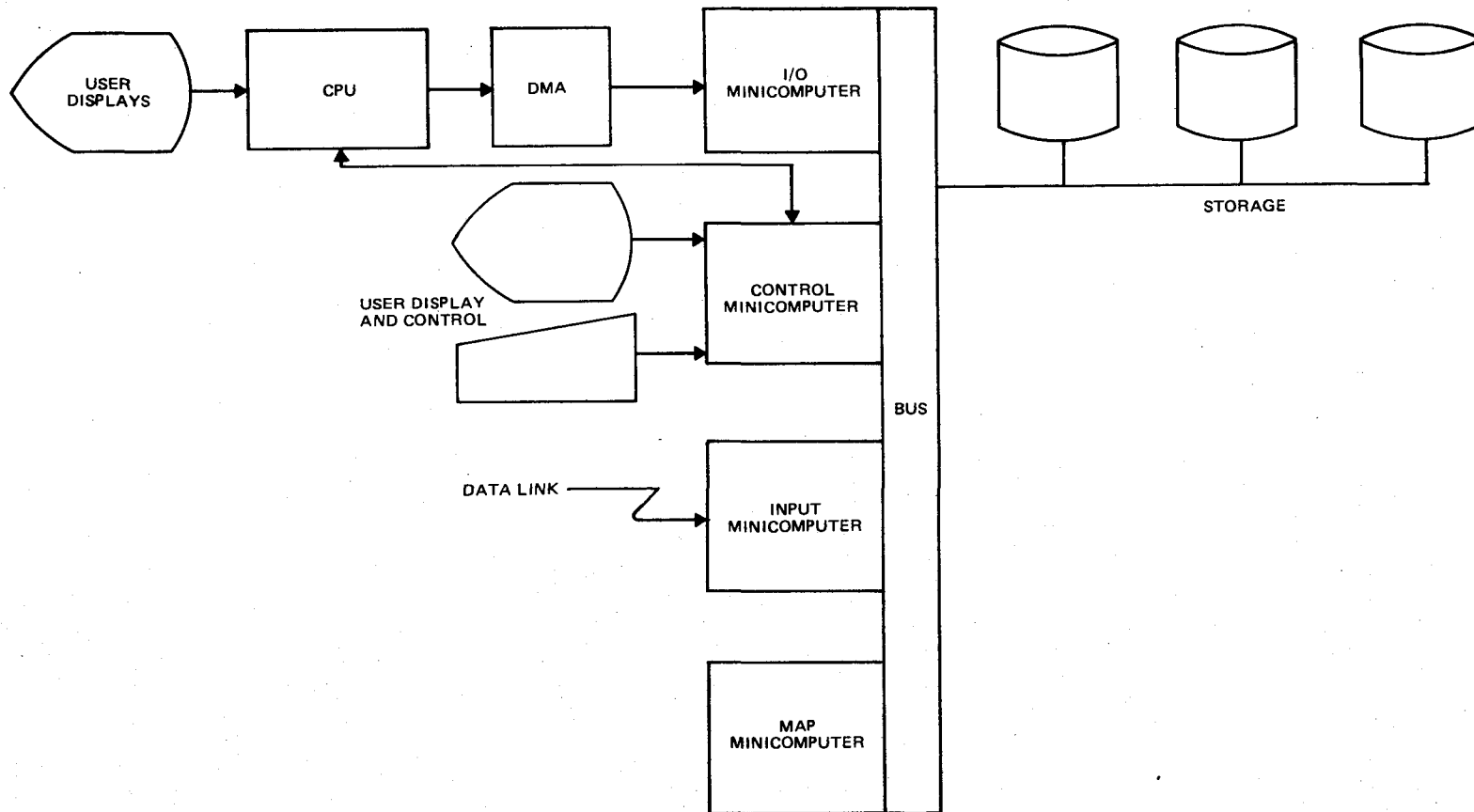


Figure D-3. Large-Scale Computer Implementation Where Either CPU or Minicomputer Controls System

APPENDIX E - LISTINGS OF TEST AND EVALUATION PROGRAMS

E.1 SUMMARY

This appendix contains listings of FORTRAN programs and subroutines used for testing and evaluating the various transformations and procedures covered in this report.

<u>Listing</u>	<u>Section</u>
Program used for evaluating coefficients of $f(x, y)$	E.2
Program used for evaluating coefficients of $f^*(\xi, \eta)$	E.3
Minimizer subroutine used by the programs of Sections E.2 and E.3	E.4
Subroutine used for generating a great circle arc	E.5
Subroutines used for mapping a point in Cartesian space into data base coordinates	E.6
Subroutines used for simulating the fast-filling method	E.7
Subroutines used for testing I/O handling method	E.8
Subroutines used for retrieving data from the data base and for graphic display	E.9

E.2 PROGRAM USED FOR EVALUATING COEFFICIENTS OF $f(x, y)$

```

C      MAIN
C
C      THIS PROGRAM COMPUTES COEFFICIENTS OF THE DIRECT TRANSFORMATION
C      FUNCTION BY MINIMIZING THE DIFFERENCE IN AREA FOR SMALL
C      AREAS
C
C      PROGRAMMER - E. MICHAEL O'NEILL
C                  COMPUTER SCIENCES CORPORATION
C                  8728 COLESVILLE RD. SILVER SPRING, MD.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      EXTERNAL FUNK
C      COMMON RM,RO,GAMMA,OMGAM,XM,YM,XIN,YIN,DX,DY,DELTA,OMEGA
C      COMMON /BILBO/ CHISO,X(20),XMIN(20),XMAX(20),DELTAX(20),
C      & DELMIN(20),ERR(20,20),NV,NTRACE,MATRIX,MASK(20)
C      COMMON /ERDDO/ NFMAX,NFLAT,JVARY,NEXTRA
C      DATA PI/3.141592653589D0/
C      DATA NOUT2/10/
C      SET PRECALCULATED COEFFICIENTS
C      DELTA=0.7904864491208D0
C      GAMSQ=PI/6.0D0
C      GAMMA=DSQRT(GAMSQ)
C      OMGAM=1.0D0-GAMMA
C      AMU=DSQRT(DSQRT(3.0D0)*PI/2.0D0)
C      SET DIMENSIONAL PARAMETERS
C      RM=1.0D0
C      RO=DSQRT(RM*RM/3.0D0)
C      R2=RO*RO
C      R4=R2*R2
C      OMEGA=0.5D0/R4*(3.0D0-2.0D0*GAMMA-AMU-2.0D0*DELTA*R4)
C      XM=RO
C      YM=RO
C      XIN=XM/ 5.0D0
C      YIN=XIN
C      DX=XM*1.0D-12
C      DY=DX
C      WRITE(NOUT2,1001)
1001  FORMAT(' INITIAL CONDITION OUTPUT, '
C      1 'ALL VARIABLE PARAMETERS ZEROED./')
C      COMPUTE AND DISPLAY INITIAL AREAS
C      CALL DISPSQ(6)
C      CALL DISPSQ(NOUT2)
C      101 CONTINUE
C      READ INITIAL VALUES AND LIMITS FROM CARDS
C      READ(5,1,END=99) NV,NFMAX,NTRACE,MATRIX,MASK
C      WRITE(6,2)NV, NFMAX, NTRACE, MATRIX,MASK
C      1 FORMAT(4I4,4X,20I1)
C      2 FORMAT(' NV, NFMAX, NTRACE, MATRIX, MASK ',4I4,4X,20I1)
C      READ(5,5) (X(I),I=1,NV)
C      WRITE(6,6) (X(I),I=1,NV)
C      READ(5,5) (XMAX(I),I=1,NV)
C      WRITE(6,6) (XMAX(I),I=1,NV)
C      READ(5,5) (XMIN(I),I=1,NV)
C      WRITE(6,6) (XMIN(I),I=1,NV)
C      READ(5,5) (DELTAX(I),I=1,NV)
C      WRITE(6,6) (DELTAX(I),I=1,NV)
C      READ(5,5) (DELMIN(I),I=1,NV)
C      WRITE(6,6) (DELMIN(I),I=1,NV)
C      5 FORMAT(10F8.3)
C      6 FORMAT(1X,10F8.3)
C      CALL DISPSQ(6)
C
C      CALL STEPIT TO MINIMIZE RMS AREA DEVIATIONS AS CALCULATED
C      BY SUBROUTINE FUNK
C
C      CALL STEPIT(FUNK)
C      DISPLAY RESULTS
C      CALL DISPSQ(6)
C      WRITE(NOUT2,1002) CHISO,(X(I),I=1,NV)
1002  FORMAT(' CHISO,VARIABLE PARAMETERS ',D12.5/,(3D21.14/))
C      CALL DISPSQ(NOUT2)
C      GO TO 101
C      99 CONTINUE
C      STOP
C      END
C      BLOCK DATA
C      INITIALIZE STEPIT COMMON AREAS
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /BILBO/ CHISO,X(20),XMIN(20),XMAX(20),DELTAX(20),
C      & DELMIN(20),ERR(20,20),NV,NTRACE,MATRIX,MASK(20)
C      DATA X/20*0.0D0/, XMAX/20*0.1D-10/, XMIN/20*0.1D-10/,
C      * DELTAX/20*0.1D-11/, DELMIN/20*0.1D-13/
C      END

```

00010000

CCCC

საქართველო

C

C

	SUBROUTINE CNTARY(SA)	00006600
C	THIS SUBROUTINE CALCULATES THE PROJECTED AREAS OF A GRID OF	
C	SMALL SQUARES BY FIRST APPLYING THE DIRECT TRANSFORMATION	
C	TO A SET OF POINTS, COMPUTING THE AREA OF THE TRANSFORMED SQUARE	
C	AND PROJECTING TO THE SURFACE OF THE SPHERE	
	IMPLICIT REAL*8 (A-H,O-Z)	00006700
	COMMON RM,RO,GAMMA,OMGAM,XM,YM,XIN,YIN,DX,DY	00006800
	DIMENSION P1(2), P2(2), P3(2), P4(2), SA(6,6)	00006900
		00007000
C	SPHERICAL PROJECTION FUNCTION	
C	SPROJ(A,B,C,D,E)=A*(B*B*C)/((C*C+D*D+E*E)**1.50D0)	00007100
		00007200
	X=0.0D0	00007300
	DO 10 J=1,5	00007400
	Y=0.0D0	00007500
	DO 5 I=1,J	00007600
C	DIRECT TRANSFORMATION	
	CALL XY TO PE (X,Y,RO,P1(1),P1(2))	00007700
	CALL XY TO PE (Y+DX,Y,RO,P2(1),P2(2))	00007800
	CALL XY TO PE (X+DX,Y+DY,RO,P3(1),P3(2))	00007900
	CALL XY TO PE (X,Y+DY,RO,P4(1),P4(2))	00008000
C	COMPUTE AREA OF TRANSFORMED SQUARE	
	S1=AREA(P1,P2,P3)	00008100
	S2=AREA(P1,P4,P3)	00008200
	S=S1+S2	00008300
C	PROJECT TO SPHERICAL SURFACE	
	SA(I,J)=SPROJ(S,RO,RO,P1(1),P1(2))	00008400
5	Y=Y+YIN	00008500
10	X=X+XIN	00008600
	X=0.0D0	00008700
	Y=YM	00008800
	DO 20 I=1,6	00008900
	CALL XY TO PE (X,Y,RO,P1(1),P1(2))	00009000
	CALL XY TO PE (X-DX,Y,RO,P2(1),P2(2))	00009100
	CALL XY TO PE (X-DX,Y-DY,RO,P3(1),P3(2))	00009200
	CALL XY TO PE (X,Y-DY,RO,P4(1),P4(2))	00009300
	S=AREA(P1,P2,P3)+AREA(P1,P4,P3)	00009400
	SA(I,6)=SPROJ(S,RO,RO,P1(1),P1(2))	00009500
	X=X+XIN	00009600
20	CONTINUE	00009700
	RETURN	00009800
	END	00009900

C	SUBROUTINE XY TO PE (XI,YI,R,P,E)	00013700
	DIRECT TRANSFORMATION FUNCTIONS	
	IMPLICIT REAL*8 (A-H,O-Z)	00013800
	COMMON RM,RO,GAMMA,OMGAM,XM,YM,XIN,YIN,DX,DY,DELTA,OMEGA	00013900
	COMMON /BILBO/ CHISQ,X(20),XMIN(20),XMAX(20),DELTAX(20),	00014000
	8 DELMIN(20),ERR(20,20),NV,NTRACE,MATRIX,MASK(20)	00014100
	1 EQUIVALENCE (C00,X(1)),(C10,X(2)),(C01,X(3)),	00014200
	2 (C11,X(4)),(C20,X(5)),(C02,X(6)),	00014300
	(D00,X(7)),(D01,X(8)),(D02,X(9))	00014400
	R2=R*R	00014500
	R4=R2*R2	00014600
	XSQ=XI*XI	00014700
	X3=XSQ*XI	00014800
	X4=XSQ*XSQ	00014900
	YSQ=YI*YI	00015000
	Y3=YSQ*YI	00015100
	Y4=YSQ*YSQ	00015200
	P=GAMMA*XI+(OMGAM/R2)*X3+	00015300
	1 XI*YSQ*(R2-XSQ)*(DELTA+(R2-YSQ)*(C00+C10*XSQ+C01*YSQ+	00015400
	2 C11*XSQ*YSQ+C20*X4+C02*Y4))+	00015500
	3 X3*(R2-XSQ)*(OMEGA+(R2-XSQ)*(D00+D01*XSQ+D02*X4))	00015600
	E=GAMMA*YI+(OMGAM/R2)*Y3+	00015700
	1 YI*XSQ*(R2-YSQ)*(DELTA+(R2-XSQ)*(C00+C10*YSQ+C01*XSQ+	00015800
	2 C11*YSQ*XSQ+C20*Y4+C02*X4))+	00015900
	3 Y3*(R2-YSQ)*(OMEGA+(R2-YSQ)*(D00+D01*YSQ+D02*Y4))	00016000
	RETURN	00016100
	END	00016200
C	CALCULATE THE AREA OF A TRIANGLE FORMED BY THREE CARTESIAN POINTS	
	FUNCTION AREA(P1,P2,P3)	00011900
	IMPLICIT REAL*8 (A-H,O-Z)	00012000
	DIMENSION P1(2),P2(2),P3(2)	00012100
	ASQ=(P1(1)-P2(1))**2+(P1(2)-P2(2))**2	00012200
	BSQ=(P2(1)-P3(1))**2+(P2(2)-P3(2))**2	00012300
	CSQ=(P3(1)-P1(1))**2+(P3(2)-P1(2))**2	00012400
	R=DSQRT(BSQ)	00012500
	C=DSQRT(CSQ)	00012600
	COSA=-(ASQ+BSQ-CSQ)/(2.0D0*R*C)	00012700
	CP=R*COSA	00012800
	H=BSQ-CP**2	00012900
	IF(H.LE.0.0D0) GO TO 100	00013000
	H=DSQRT(H)	00013100
	AREA=0.5D0*C*H	00013200
	RETURN	00013300
100	AREA=0.0D0	00013400
	RETURN	00013500
	END	00013600

E.3 PROGRAM USED FOR EVALUATING COEFFICIENTS OF $f^*(\xi, \eta)$

```

C      MAIN
C      THIS PROGRAM COMPUTES THE COEFFICIENTS OF THE INVERSE
C      TRANSFORMATION FUNCTION BY MINIMIZING THE DEVIATIONS OF
C      A RETRANSFORMED GRID
C      PROGRAMMER - E. MICHAEL O'NEILL
C                  COMPUTER SCIENCES CORPORATION
C                  8728 COLFESVILLE RD. SILVER SPRING, MD.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      EXTERNAL FUNK
C      COMMON RS,R,RSQ,R4,XIN,YIN
C      COMMON/FRODO/ NFMAX,NFLAT,JVARY,NEXTRA
C      COMMON /BILBO/ DIFF,VAR(20),VMIN(20),VMAX(20),DV(20),
C      1      DELMIN(20),ERR(20,20),NV,NT,MAT,MASK(20)
C      SET DIMENSIONAL CONSTANTS
C      RS=1.0D0
C      R=0.5773502691896D0
C      RSQ=0.333333333333333D0
C      R4=0.111111111111111D0
C      INITIALIZE COEFFICIENTS
C      DO 10 I=1,20
C      VAR(I)=0.0D0
C      VMIN(I)=-0.5D3
C      VMAX(I)= 0.5D3
C      DV(I)=0.1D0
C      DELMIN(I)=0.1D-10
C 10  MASK(I)=0
C      NUMBER OF COEFFICIENTS
C      NV=13
C      NUMBER OF ITERATIONS
C      NFMAX=2000
C      NT=0
C      MAT=0
C      XIN=R/5.0D0
C      YIN=XIN
C
C      STEPIT CALLS SUBROUTINE FUNK WHICH CALCULATES THE RMS
C      DEVIATION OF THE RETRANSFORMED GRID, STEPIT ITERATES UNTIL
C      A SATISFACTORY RMS HAS BEEN REACHED OR UNTIL NFMAX ITERATIONS
C      CALL STEPIT(FUNK)
C      USE FINAL COEFFICIENTS TO CALCULATE RETRANSFORMED GRID AND PRINT
C
C      X=0.0D0
C      DO 20 IX=1,6
C      Y=0.0D0
C      DO 15 IY=1,IX
C      DIRECT TRANSFORMATION
C      P=FDMAP(X,Y)
C      E=FDMAP(Y,X)
C      INDIRECT TRANSFORMATION
C      XB=FIAP(P,E)
C      YB=FIAP(E,P)
C      DIFF=(X-XB)**2+(Y-YB)**2
C      WRITE(6,12) X,Y,P,E,XB,YB,DIFF
C      WRITE(1,12) X,Y,P,E,XB,YB,DIFF
C 12  FORMAT(' X,Y,P,E,XB,YB,DIFF ',7F8.5)
C 15  Y=Y+YIN
C 20  X=X+XIN
C      STOP
C      END

```

C	SUBROUTINE FUNK	00007000
C	THIS SUBROUTINE CALCULATES THE SUM OF THE SQUARES OF THE	
C	DEVIATIONS OF THE RETRANSFORMED GRID	
C	IMPLICIT REAL*8 (A-H,O-Z)	00007100
	COMMON/RILBO/ DIFF,VAR(20)	00007200
	COMMON RS,R,RSQ,R4,XIN,YIN	00007300
	DIFF=0.000	00007400
	X=0.000	00007500
	DO 10 IX=1,6	00007600
	Y=0.000	00007700
	DO 5 IY=1,IX	00007800
C	DIRECT TRANSFORMATION	
	P=FDMAP(X,Y)	00007900
	E=FDMAP(Y,X)	00008000
C	INVERSE TRANSFORMATION	
	XB=FIMAP(P,E)	00008100
	YB=FIMAP(E,P)	00008200
	DIFF=DIFF+(X-XB)**2+(Y-YB)**2	00008300
5	Y=Y+YIN	00008400
10	X=X+XIN	00008500
	RETURN	00008600
	END	00008700

	FUNCTION FDMAP(A,B)	00005500
C	THIS FUNCTION EVALUATES THE DIRECT TRANSFORMATION AT A,B USING	
C	A PREDETERMINED SET OF COEFFICIENTS	
C		
	IMPLICIT REAL *8 (A-H,O-Z)	00005600
	COMMON RS,R,RSQ,R4,XIN,YIN	00005700
	DATA GAMMA,OMGAM/0.7236012545582D0,0.2763987454418D0/	00005710
	DATA DELTA,OMEGA/0.7904864491208D0,-0.1225441487984D1/	00005720
	DATA C00,C10,C01/-0.272170536D1,-0.558421683D1,0.217111748D1/	00005730
	DATA C11,C20,C02/-0.641601515D1,-0.345786274D1,0.197362657D1/	00005740
	DATA D0,D1,D2/0.148331292D1,0.111997260D1,0.605153821D1/	00005750
	ASQ=A*A	00005800
	A3=A*ASQ	00005900
	A4=ASQ*ASQ	00006000
	BSQ=B*B	00006100
	B4=BSQ*BSQ	00006200
	RMA=RSQ-ASQ	00006300
	FDMAP=GAMMA*A+OMGAM/RSQ*A3+	00006400
1	A3*RMA*(OMEGA+RMA*(D0+D1*ASQ+D2*A4))+	00006500
2	A*BSQ*RMA*(DELTA+(RSQ-BSQ)*	00006600
3	(C00+C10*ASQ+C01*BSQ+C11*ASQ*BSQ+C20*A4+C02*B4))	00006700
	RETURN	00006800
	END	00006900
	FUNCTION FIMAP(A,B)	00004200
C	THIS FUNCTION EVALUATES THE INVERSE TRANSFORMATION USING A	
C	SET OF COEFFICIENTS INPUTTED THROUGH COMMON/BILBO/	
C		
	IMPLICIT REAL *8 (A-H,O-Z)	00004300
	COMMON RS,R,RSQ,R4,XIN,YIN	00004400
	COMMON/BILBO/ DIF,VAR(20)	00004500
	EQUIVALENCE (DELTA,VAR(1)),(OMEGA,VAR(2)),	00004525
1	(DELT1,VAR(3)),(OMEG1,VAR(4)),	00004550
1	(C00,VAR(5)),(C10,VAR(6)),(C01,VAR(7)),	00004600
1	(C11,VAR(8)),(C20,VAR(9)),(C02,VAR(10)),	00004650
1	(D0,VAR(11)),(D1,VAR(12)),(D2,VAR(13))	00004700
	DATA GAMMA,OMGAM/0.1381976597886D1,-0.3819765978855D0/	00004805
	ASQ=A*A	00004810
	A3=A*ASQ	00004815
	A4=ASQ*ASQ	00004820
	BSQ=B*B	00004825
	B4=BSQ*BSQ	00004830
	RMA=RSQ-ASQ	00004835
	RMA=RSQ-ASQ	00004900
	FIMAP=GAMMA*A+OMGAM/RSQ*A3+	00005000
1	A3*RMA*(OMEGA+OMEG1*(RSQ-BSQ)+RMA*(D0+D1*ASQ+D2*A4))+	00005100
2	A*BSQ*RMA*(DELTA+DELT1*RMA+(RSQ-BSQ)*	00005150
3	(C00+C10*ASQ+C01*BSQ+C11*ASQ*BSQ+C20*A4+C02*B4))	00005200
	RETURN	00005300
	END	00005400

E.4 MINIMIZER SUBROUTINE USED BY THE PROGRAMS OF SECTIONS E.2 AND E.3

```

SUBROUTINE STEPIT %FUNK<
IMPLICIT REAL*8 (A-H,O-Z)

360 STEPIT, MODIFIED BY J. BENSINGER, U. PENNSYLVANIA, 1971
STEPIT FINDS LOCAL MINIMA OF A SMOOTH FUNCTION OF SEVERAL PARAMETERS.
@STEPIT IS A PHLEGMATIC METHOD OF SOLVING A PROBLEM.@
-- J. H. BURRILL, JR., @360 STEPIT - A USER@S MANUAL@
THIS SOURCE DECK AND A LONG WRITE-UP ARE AVAILABLE FROM ....

QUANTUM CHEMISTRY PROGRAM EXCHANGE
DEPT. OF CHEMISTRY, INDIANA UNIVERSITY
BLOOMINGTON, INDIANA 47401

* * * * *
FUNK      -- THE NAME OF THE SUBROUTINE THAT COMPUTES CHISO
            GIVEN X%1<,X%2<,...,X%NV<
NV         -- THE NUMBER OF PARAMETERS, X
NTRACE    -- #0 FOR NORMAL OUTPUT, #&1 FOR TRACE OUTPUT,
            #-1 FOR NO OUTPUT
MATRIX    -- #0 FOR NO ERROR CALCULATION, #100&M FOR ERROR
            CALCULATION USING STEPS 10**M TIMES LARGER
            THAN THE LAST STEPS USED IN THE MINIMIZATION
CHISO     -- THE VALUE OF THE FUNCTION TO BE MINIMIZED
MASK%J<   -- NONZERO IF X%J< IS TO BE HELD FIXED
X%J<      -- THE J-TH PARAMETER
XMAX%J<   -- THE UPPER LIMIT ON X%J<
XMIN%J<   -- THE LOWER LIMIT ON X%J<
DELTA%J<  -- THE INITIAL STEP SIZE FOR X%J<
DELMIN%J< -- THE LOWER LIMIT %CONVERGENCE TOLERANCE< ON THE
            STEP SIZE FOR X%J<
ERR%J,K<  -- RETURNS THE ERROR MATRIX %ALSO USED FOR SCRATCH
            STORAGE<
NFMAX     -- THE MAXIMUM NUMBER OF FUNCTION COMPUTATIONS
NFLAT     -- NONZERO IF THE SEARCH IS TO TERMINATE WHEN ALL
            TRIAL STEPS GIVE IDENTICAL FUNCTION VALUES
JVARY     -- STEPIT SETS JVARY NONZERO IF X%JVARY< IS THE ONLY
            X%J< THAT HAS CHANGED SINCE THE LAST CALL TO
            FUNK
NEXTRA    -- USED BY SUBROUTINE SIMPLEX BUT NOT BY STEPIT

* * * * *
THE DIMENSIONS OF ALL VECTORS AND MATRICES ARE NV, EXCEPT FOR ....
ERR%NV,MAX%NV,MOSQUE<<,SECOND%2,2<,XOSC%NV,MOSQUE<,CHIOSC%MOSQUE<.
TO REDUCE STORAGE TO A MINIMUM, SET MOSQUE#0, REDIMENSION ERR%1,1<,
XOSC%1,1<, SALVO%1<, AND CHIOSC%1<, AND DELETE THE OSCILLATION
SEARCH AND ERROR COMPUTATION SECTIONS %SEE COMMENT CARDS BELOW<.
OR, USE SUBROUTINE STP, WHICH HAS THESE DELETIONS PLUS DELETION OF
THE COLINEARITY CHECK.

* * * * *
COMMON /BILBO/ CHISO,X(20),XMIN(20),XMAX(20),DELTA(20),
& DELMIN(20),ERR(20,20),NV,NTRACE,MATRIX,MASK(20)

COMMON /FRODO/ NFMAX,NFLAT,JVARY,NEXTRA

DIMENSION VEC%20<,TRIAL%20<,XSAVE%20<,CHI%20<,DX%20<,SECOND%2,2<
DIMENSION OLDVEC%20<,SALVO%20<,XOSC%20,15<,CHIOSC%15<,JFLAT%20<

TO RUN ON THE CDC 3600, THE FOLLOWING DATA STATEMENT MUST BE
ACTIVATED AND SUBROUTINE SSWTCH MUST BE SUPPLIED.
TO RUN ON OTHER COMPUTERS, A BLOCK DATA SUBPROGRAM MUST BE SUPPLIED
TO SET NFMAX AND NFLAT.

DATA %NFMAX#1000000<,%NFLAT#1<

* * * * *
SET FIXED QUANTITIES ....

KW ... STANDARD OUTPUT UNIT NUMBER
IBM 709/7090/7094 ....
CDC 3600/6400 ....
KTYPE .... CONSOLE TYPEWRITER UNIT

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```

C      XMIN%I<#-HUGE
C      NACTIV#NACTIV&1
C      IF%I<#-XMAX%I<<210,210,200
C      X%I<#AMAX1%XMIN%I<,AMIN1%XMAX%I<,X%I<<<
C      IF%I<#XMAX%I<
C      IF%I<#XMIN%I<<220,230,230
C      X%I<#XMIN%I<
C      CONTINUE
C      COMPUTE COMPAR. THE PROBABILITY THAT THE COSINE OF THE ANGLE
C      BETWEEN TWO RANDOM DIRECTIONS EXCEEDS COMPAR IS APPROXIMATELY
C      %1-COLIN</2 .
C      COMPAR#0.0
C      IF%NACTIV-1<240,300,260
C      DO 250 J#1,NV
C      MASK%J<#0
C      GO TO 50
C      A#NACTIV
C      SUB#2.0/%A-1.0<
C      P#2.0*%1.0/SQRT %A</%1.0-0.5**SUB<-1.0<
C      P#2.0*%1.0/DSQRT%A</%1.0-0.5**SUB<-1.0<
C      COMPAR#%1.-%1.-COLIN<**SUB<*%1.6P*%1.-COLIN<<
C      COMPAR#MIN1F%.999,ABSF%COMPAR<<
C      IF%COMPAR<270,280,280
C      COMPAR#-COMPAR
C      IF%COMPAR-.999<300,300,290
C      COMPAR#.999
C      IF%NTRACE<390,310,310
C      WRITE% KW,320<
C      FORMAT%92H1ENTER SUBROUTINE STEPIT. ORIGINAL VERSION BY CHANDLER
C      *, PHYSICS DEPT., INDIANA UNIVERSITY.//19H INITIAL VALUES..../<
C      WRITE% KW,330<%MASK%J<,J#1,NV<
C      FORMAT%/10H MASK # 9#I6.6X</%4X9I12<<
C      WRITE% KW,340<%X%J<,J#1,NV<
C      FORMAT%/10H X # 9E12.4/%10X 9E12.4<<
C      WRITE% KW,350<%XMAX%J<,J#1,NV<
C      FORMAT%/10H XMAX # 9E12.4/%10X 9E12.4<<
C      WRITE% KW,360<%XMIN%J<,J#1,NV<
C      FORMAT%/10H XMIN # 9E12.4/%10X 9E12.4<<
C      WRITE% KW,370<%DELTA%J<,J#1,NV<
C      FORMAT%/10H DELTA # 9E12.4/%10X 9E12.4<<
C      WRITE% KW,380<%DELMIN%J<,J#1,NV<
C      FORMAT%/10H DELMIN # 9E12.4/%10X 9E12.4<<
C      CALL FUNK
C      CHISAV#CHISQ
C      CALL FUNK
C      NF ... NUMBER OF FUNCTION CALLS
C      NF#2
C      IF%CHISQ-CHISAV<400,420,400
C      WRITE %KW,410< CHISAV,CHISQ,NF
C      FORMAT%//3%/59H WARNING.... CHISQ IS NOT A REPRODUCIBLE FUNCTION
C      * OF X%J<. <A5X 9HCHISAV # E22.14,5X 8HCHISQ # E22.14,5X5HNF # I5<
C      JOCK ... SWITCH USED IN SETTING JVARY
C      JOCK#1
C      IF%NTRACE<450,430,430
C      WRITE% KW,440<NV,NACTIV,MATRIX,NCOMP,NFMAX,NFLAT,
C      * RATIO,ACK,COLIN,COMPAR,CHISQ
C      FORMAT%/1H I3,11H VARIABLES,I3,8H ACTIVE.10X8HMATRIX #I4,10X7HNC
C      *MP #I2,10X7HNFMAX #I8,10X7HNFAT #I2//
C      * 8H RATIO #F5.1,10X5HACK #F5.1,10X7HCOLIN #F6.3,10X8HCOMPARGR
C      * #F6.3//8H CHISQ #E15.8//23H BEGIN MINIMIZATION.... <
C      IF%NV<2120,2120,460
C      IF%NTRACE<490,490,470
C      WRITE% KW,480<
C      FORMAT%/60%1X1H*<//10X37HTRACE MAP OF THE MINIMIZATION PROCESS//<
C      DO 500 I#1,NV
C      VEC%J< ... CURRENT VECTOR OF NUMBER OF
C      STEPS IN X%J<
C      VEC%I<#0.
C      DX%J< ... CURRENT STEP SIZE FOR X%J<
C      500 DX%I<#DELTA%I<
C      CHIOLD#CHISQ
C      CHIOLD ... BEST PREVIOUS VALUE OF CHISQ
C      NOSC ... CURRENT DEPTH OF THE OSCILLATION
C      INFORMATION
C      NOSC#0
C      KWIT ... TERMINATION SWITCH
C      KWIT#0
C      * * * * *

```

```

C VARY THE PARAMETERS ONE AT A TIME.
C THIS IS THE STARTING POINT USED EACH TIME THE STEP SIZE IS REDUCED
C OR A SUCCESSFUL GIANT STEP IS COMPLETED.
C NCIRC ... NUMBER OF CONSECUTIVE X%J<
C WITHOUT SIZEABLE CHANGES
510 NCIRC#0
C NZIP ... NUMBER OF CONSECUTIVE CYCLES
C WITHOUT A GIANT STEP
C NZIP#0
C MAIN DO LOOP FOR CYCLING THROUGH THE VARIABLES.
C FIRST TRIAL STEP WITH EACH VARIABLE IS SEPARATE.
C NACK ... NUMBER OF ACTIVE X%J< CYCLED
C THROUGH
520 NACK#0
C DO 1750 I#1,NV
C JFLAT%J< ... NONZERO IF CHANGING X%J< DID
C NOT CHANGE CHISQ
C JFLAT%I<#0
C OLDVEC%J< ... OLD VECTOR OF NUMBER OF
C STEPS IN X%J<
C OLDVEC%I<#VEC%I<
C VEC%I<#0.0
C TRIAL%J< ... CHANGE IN X%J<
C IF%MASK%I<<530,540,530
530 VEC%I<#-0.0
C JFLAT%I<#1
C GO TO 1730
540 NACK#NACK&1
C SAVE%X%I<
C CHECK THAT DX%I< IS NOT NEGLIGIBLE.
C DELX#DX%I<
C IF%DELX*SAVE<550,560,560
550 DELX#-DELX
560 XPLUS#SAVE&DELX
C IF%XPLUS-SAVE<580,570,580
570 JFLAT%I<#2
C GO TO 770
C ADX#ABS%DX%I<<
580 ADX#DX%I<
C IF%ADX<590,600,600
590 ADX#-ADX
C STEP X%I<.
600 X%I<#SAVE&DX%I<
C JVARY#0
C IF%JOCK<620,620,610
610 JOCK#0
C JVARY#1
620 NFLAG#1
C IF%X%I<-XMIN%I<<640,630,630
630 IF%X%I<-XMAX%I<<650,650,640
640 NFLAG#NFLAG&3
C GO TO 670
650 CALL FUNK
C NF#NF&1
C JVARY#1
C SAVE OLD VALUE OF CHISQ FOR INTERPOLATION.
C CHIME#CHISQ
C IF%CHISQ-CHIOLD<810,660,670
660 NFLAG#NFLAG&1
C STEP X%I< THE OTHER WAY.
670 X%I<#SAVE-DX%I<
C IF%X%I<-XMIN%I<<780,680,680
680 IF%X%I<-XMAX%I<<690,690,780
690 CALL FUNK
C NF#NF&1
C JVARY#1
C IF%CHISQ-CHIOLD<800,700,710
700 NFLAG#NFLAG&1
710 IF%NFLAG-3<720,760,780
C PERFORM PARABOLIC INTERPOLATION.
C CHECK FOR ZERO DENOMINATOR, ETC.
720 IF%XCHISQ-CHIME<%XCHIME-2.*CHIOLD&CHISQ<<730,780,730
730 TRIAL%I<#5*DX%I<*&XCHISQ-CHIME</%CHIME-2.*CHIOLD&CHISQ<
C VEC%I<#TRIAL%I</ADX
C X%I<#SAVE&TRIAL%I<
C CALL FUNK
C NF#NF&1
C IF%CHISQ-CHIOLD<740,750,750
GRH04190
GRH041A0
GRH041B0
GRH041C0
GRH041D0
GRH041E0
GRH041F0
GRH04200
GRH04210
GRH04220
GRH04230
GRH04240
GRH04250
GRH04260
GRH04270
GRH04280
GRH04290
GRH042A0
GRH042B0
GRH042C0
GRH042D0
GRH042E0
GRH042F0
GRH04300
GRH04310
GRH04320
GRH04330
GRH04340
GRH04350
GRH04360
GRH04370
GRH04380
GRH04390
GRH043A0
GRH043B0
GRH043C0
GRH043D0
GRH043E0
GRH043F0
GRH04400
GRH04410
GRH04420
GRH04430
GRH04440
GRH04450
GRH04460
GRH04470
GRH04480
GRH04490
GRH044A0
GRH044B0
GRH044C0
GRH044D0
GRH044E0
GRH044F0
GRH04500
GRH04510
GRH04520
GRH04530
GRH04540
GRH04550
GRH04560
GRH04570
GRH04580
GRH04590
GRH045A0
GRH045B0
GRH045C0
GRH045D0
GRH045E0
GRH045F0
GRH04600
GRH04610
GRH04620
GRH04630
GRH04640
GRH04650
GRH04660
GRH04670
GRH04680
GRH04690
GRH046A0
GRH046B0
GRH046C0

```

```

740 CHIOLD#CHISQ
JOCK#1
GO TO 790
750 TRIAL#I<#0.0
VEC#I<#0.0
GO TO 780
760 JFLAT#I<#1
770 VEC#I<#-0.
780 X#I<#SAVE
790 NCIRC#NCIRC&1
IF#NCIRC-NACTIV<910,1820,1820
C RESET DX#I< FOR MORE EFFICIENT OPERATION.
800 DX#I<#-DX#I<
C
C A LOWER VALUE OF CHISQ HAS BEEN FOUND. STEP, DOUBLE THE STEP SIZE,
C AND REPEAT AS LONG AS CHISQ CONTINUES TO DECREASE.
C
810 NCIRC#0
DEL#DX#I<
NSTP#0
820 CHIME#CHIOLD
CHIOLD#CHISQ
C VEC#I<#VEC#I<&DEL/ABS %DX#I<<
VEC#I<#VEC#I<&DEL/DABS%DX#I<<
TRIAL#I<#TRIAL#I<&DEL
NSTP#NSTP&1
IF#NSTP-NSTPMX<830,890,890
830 DEL#ACK#DEL
SAVE#X#I<
X#I<#SAVE&DEL
IF#X#I<-XMIN#I<<900,840,840
840 IF#X#I<-XMAX#I<<850,850,900
850 CALL FUNK
NF#NF&1
IF#CHISQ-CHIOLD<820,860,860
C PERFORM PARABOLIC INTERPOLATION.
860 DENOM#ACK#CHIME-%ACK&1.<#CHIOLD&CHISQ
IF#DENOM<870,900,870
870 CINDER#%.5/ACK<#ACK**2*CHIME-%ACK**2-1.<#CHIOLD-CHISQ/DENOM
X#I<#SAVE&CINDER#DEL
CALL FUNK
NF#NF&1
IF#CHISQ-CHIOLD<880,900,900
880 CHIOLD#CHISQ
TRIAL#I<#TRIAL#I<&CINDER#DEL
VEC#I<#VEC#I<&CINDER#DEL/ADX
890 JOCK#1
GO TO 910
900 X#I<#SAVE
C DO NOT INCREASE THE STEP SIZE PREMATURELY.
910 IF#NZIP<920,920,940
920 IF#NCOMP-1<930,930,1720
930 IF#NACK-1<1720,1720,940
C AVEL#ABS%VEC#I<<
940 AVEC#VEC#I<
IF#AVEC<950,960,960
950 AVFC#-AVFC
960 IF#AVFC-FACUP<1030,970,970
970 DX#I<#ACK#ADX
VEC#I<#VEC#I</ACK
OLDVEC#I<#OLDVEC#I</ACK
IF#NOSC<1000,1000,980
980 DO 990 J#1,NOSC
990 ERR#I,J<#ERR#I,J</ACK
1000 IF#NTRACE<1030,1030,1010
1010 WRITE% KW,1020<I,DX#I<
1020 FORMAT%10H STEP SIZE%13,14H INCREASED TO E12.5<
C * * * * *
C IF POSSIBLE STEP ALONG A RESULTANT DIRECTION.
C
C CHECK THE COLINEARITY OF VEC AND OLDVEC.
C
1030 SUMO#0.0
SUMV#0.0
DO 1040 J#1,NV
SUMO#SUMO&OLDVEC#J<#2
SUMV#SUMV&VEC#J<#2
1040 IF#SUMO#SUMV<1720,1720,1050
C1050 SUMO#SQRT %SUMO<
1050 SUMO#DSQRT%SUMO<
C SUMV#SQRT %SUMV<
SUMV#DSQRT%SUMV<
COSINE#0.0

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GRH046D0
GRH046E0
GRH046F0
GRH04700
GRH04710
GRH04720
GRH04730
GRH04740
GRH04750
GRH04760
GRH04770
GRH04780
GRH04790
GRH047A0
GRH047B0
GRH047C0
GRH047D0
GRH047E0
GRH047F0
GRH04800
GRH04810
GRH04820
GRH04830
GRH04840
GRH04850
GRH04860
GRH04870
GRH04880
GRH04890
GRH048A0
GRH048B0
GRH048C0
GRH048D0
GRH048E0
GRH048F0
GRH04900
GRH04910
GRH04920
GRH04930
GRH04940
GRH04950
GRH04960
GRH04970
GRH04980
GRH04990
GRH049A0
GRH049B0
GRH049C0
GRH049D0
GRH049E0
GRH049F0
GRH04A00
GRH04A10
GRH04A20
GRH04A30
GRH04A40
GRH04A50
GRH04A60
GRH04A70
GRH04A80
GRH04A90
GRH04AA0
GRH04AB0
GRH04AC0
GRH04AD0
GRH04AE0
GRH04AF0
GRH04B00
GRH04B10
GRH04B20
GRH04B30
GRH04B40
GRH04B50
GRH04B60
GRH04B70
GRH04B80
GRH04B90
GRH04BA0
GRH04BB0
GRH04BC0
GRH04BD0
GRH04BE0
GRH04BF0
GRH04C00

```

[illegible]

C	PERFORM GIGANTIC OR GIANT STEPS.	GRH05150
C		GRH05160
1300	CHIBAK#CHI#I<	GRH05170
1310	DO 1360 J#1,NV	GRH05180
	XSAVE#J<#X#J<	GRH05190
	TRIAL#J<#ACK*TRIAL#J<	GRH051A0
	IF#MASK#J<<1360,1320,1360	GRH051B0
1320	X#J<#X#J<#TRIAL#J<	GRH051C0
C	X#J<#AMAX1#AMIN1#X#J<,XMAX#J<,XMIN#J<<	GRH051D0
	IF#X#J<-XMAX#J<<1340,1340,1330	GRH051E0
1330	X#J<#XMAX#J<	GRH051F0
1340	IF#X#J<-XMIN#J<<1350,1360,1360	GRH05200
1350	X#J<#XMIN#J<	GRH05210
1360	CONTINUE	GRH05220
	JOCK#0	GRH05230
	JVARY#0	GRH05240
	CALL FUNK	GRH05250
	NF#NF&1	GRH05260
	IF#CHISQ-CHIOLO<1370,1440,1440	GRH05270
1370	CHIBAK#CHIOLO	GRH05280
	CHIOLO#CHISQ	GRH05290
	NGIANT#NGIANT&1	GRH052A0
	IF#NTRACE<1310,1310,1380	GRH052B0
1380	IF#NGIANT-1<1390,1390,1420	GRH052C0
1390	WRITE# KW,1400<CHIBAK,NF,#VEC#J<,J#1,I<	GRH052D0
1400	FORMAT#//8H CHISQ #F16.8,8X4HNF #I7//5X16HNO. OF STEPS # 9E11.3/	GRH052E0
	* 21X9E11.3<<	GRH052F0
	WRITE# KW,1410<#XSAVE#J<,J#1,NV<	GRH05300
1410	FORMAT#9H X#I<.../X1X9E13.5<<	GRH05310
1420	WRITE# KW,1430<CHISQ,NF,#X#J<,J#1,NV<	GRH05320
1430	FORMAT#//8H CHISQ #E16.8,8X4HNF #I7/9H X#I<.../X1X9E13.5<<	GRH05330
	GO TO 1310	GRH05340
C	DO NOT INTERPOLATE AFTER AN UNSUCCESSFUL	GRH05350
C	GIANT STEP.	GRH05360
1440	IF#NGIANT<1530,1530,1450	GRH05370
C	PERFORM PARABOLIC INTERPOLATION.	GRH05380
1450	DENOM#ACK*CHIBAK-#ACK&1.<#CHIOLO&CHISQ	GRH05390
	IF#DENOM<1460,1520,1460	GRH053A0
1460	CINDER#%.5/ACK<#ACK**2*CHIBAK-#ACK**2-1.<#CHIOLO-CHISQ/>DENOM	GRH053B0
	DO 1510 J#1,NV	GRH053C0
	IF#MASK#J<<1510,1470,1510	GRH053D0
1470	X#J<#XSAVE#J<#CINDER*TRIAL#J<	GRH053E0
C	X#J<#AMAX1#AMIN1#X#J<,XMAX#J<,XMIN#J<<	GRH053F0
	IF#X#J<-XMAX#J<<1490,1490,1480	GRH05400
1480	X#J<#XMAX#J<	GRH05410
1490	IF#X#J<-XMIN#J<<1500,1510,1510	GRH05420
1500	X#J<#XMIN#J<	GRH05430
1510	CONTINUE	GRH05440
	JOCK#0	GRH05450
	JVARY#0	GRH05460
	CALL FUNK	GRH05470
	NF#NF&1	GRH05480
	IF#CHISQ-CHIOLO<1650,1520,1520	GRH05490
1520	IF#NGIANT<1560,1530,1560	GRH054A0
1530	IF#NTRY<1540,1560,1540	GRH054B0
1540	DO 1550 J#1,NV	GRH054C0
	TRIAL#J<#SALVO#J<	GRH054D0
1550	X#J<#XSAVE#J<	GRH054E0
	GO TO 1580	GRH054F0
1560	DO 1570 J#1,NV	GRH05500
	TRIAL#J<#TRIAL#J</ACK	GRH05510
1570	X#J<#XSAVE#J<	GRH05520
1580	IF#NTRACE<1610,1610,1590	GRH05530
1590	WRITE# KW,1600<CHIOLO,NGIANT	GRH05540
1600	FORMAT#//8H CHISQ #E15.8,7H AFTERI3,13H GIANT STEPS. <	GRH05550
	WRITE# KW,1410<#X#J<,J#1,NV<	GRH05560
1610	IF#NGIANT<1620,1620,1680	GRH05570
1620	IF#NRETRY<1630,1630,1220	GRH05580
1630	IF#NTRY<1640,1700,1640	GRH05590
C	ALL GIGANTIC STEPS WERE UNSUCCESSFUL.	GRH055A0
C	TRY A GIANT STEP.	GRH055B0
1640	NTRY#0	GRH055C0
	GO TO 1300	GRH055D0
C		GRH055E0
1650	CHIOLO#CHISQ	GRH055F0
	JOCK#1	GRH05600
	IF#NTRACE<1680,1680,1660	GRH05610
1660	STEPS#NGIANT	GRH05620
	STEPS#STEPS&CINDER	GRH05630
	WRITE# KW,1670<CHIOLO,STEPS	GRH05640
1670	FORMAT#//8H CHISQ #E15.8,7H AFTERF6.1,13H GIANT STEPS. <	GRH05650
	WRITE# KW,1410<#X#J<,J#1,NV<	GRH05660
1680	IF#NTRY<1690,510,1690	GRH05670
1690	CONTINUE	GRH05680

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C          A SUCCESSFUL GIGANTIC STEP HAS OCCURRED.
C          GO TO 510
C          AN UNSUCCESSFUL GIANT STEP HAS OCCURRED.
C          DELETE ITS OSCILLATION INFORMATION.
C          NOSC#MAX0%NOSC-1,0<
1700 NOSC#NOSC-1
      IF%NOSC<1710,1720,1720
1710 NOSC#0
1720 CHI%I<#CHIOLD
1730 CONTINUE
      DECOMMENT FOR SSW OPTION ....
      CALL SSWTCH %NSSW,JUMP<
      IF%JUMP-1<2090,2090,1740
1740 IF%NF-NFMAX<1750,1750,2070
1750 CONTINUE
      END OF THE MAIN DO LOOP.
      * * * * *
      ANOTHER CYCLE THROUGH THE VARIABLES HAS BEEN COMPLETED.
      PRINT ANOTHER LINE OF TRACES.
      IF%NTRACE<1770,1770,1760
1760 WRITE%      KW,1400<CHIOLD,NF,%VEC%J<,J#1,NV<
1770 IF%NZIP<1810,1780,1810
1780 IF%NTRACE<1810,1810,1790
1790 WRITE%      KW,1410<%X%J<,J#1,NV<
      WRITE%      KW,1800<
1800 FORMAT%1H<
1810 NZIP#NZIP&1
      GO TO 520
C          A MINIMUM HAS BEEN FOUND. PRINT THE REMAINING TRACES.
C          1820 IF%NTRACE<1840,1840,1830
C          1830 WRITE%      KW,1400<CHIOLD,NF,%VEC%J<,J#1,I<
C          WRITE%      KW,1410<%X%J<,J#1,NV<
C          DECREASE THE SIZE OF THE STEPS FOR ALL VARIABLES.
C          1840 CONTINUE
C          DECOMMENT FOR SSW OPTION ....
C          CALL SSWTCH %NSSW,JUMP<
C          IF%JUMP-1<2090,2090,1850
C          1850 IF%NF-NFMAX<1860,1860,2070
C          CHECK WHETHER ALL DX%J< .LE. DELMIN%J<.
C          1860 NGATE#1
C          DO 1910 J#1,NV
C          IF%MASK%J<<1910,1870,1910
C          ADX#ABS%DX%J<<
C          1870 ADX#DX%J<
C          IF%ADX<1880,1890,1890
C          1880 ADX#-ADX
C          1890 IF%ADX-DELMIN%J<<1910,1910,1900
C          1900 NGATE#0
C          1910 DX%J<#DX%J</RATIO
C          IF%NGATE<1920,1920,1960
C          CHECK THE JFLAT%J<.
C          1920 JFLMIN#5
C          DO 1950 J#1,NV
C          IF%MASK%J<<1950,1930,1950
C          1930 IF%JFLAT%J<-JFLMIN<1940,1950,1950
C          1940 JFLMIN#JFLAT%J<
C          1950 CONTINUE
C          IF%JFLMIN-1<2040,1990,1960
C          1960 IF%NTRACE<2130,1970,1970
C          1970 WRITE%      KW,1980<
C          1980 FORMAT%///65H TERMINATED WHEN THE STEP SIZES BECAME AS SMALL AS TH
C          *E DELMIN%J<. <
C          GO TO 2130
C          1990 IF%NFLAT<2040,2040,2000
C          2000 IF%NTRACE<2130,2010,2010
C          2010 WRITE%      KW,2020<
C          2020 FORMAT%///72H TERMINATED WHEN THE FUNCTION VALUES AT ALL TRIAL POI
C          *NTS WERE IDENTICAL.
C          WRITE%      KW,2030<%DX%J<,J#1,NV<
C          2030 FORMAT%///29H CURRENT STEP SIZE VALUES....//%1X9E13.5<<
C          GO TO 2130
C          2040 IF%NTRACE<510,510,2050
C          PRINT THE DX%J< AND SEARCH SOME MORE.
C          2050 WRITE%      KW,2060<%DX%J<,J#1,NV<

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GRH05BD0
GRH05BE0
GRH05BF0
GRH05C00
GRH05C10
GRH05C20
GRH05C30
GRH05C40
GRH05C50
GRH05C60
GRH05C70
GRH05C80
GRH05C90
GRH05CA0
GRH05CB0
GRH05CC0
GRH05CD0
GRH05CE0
GRH05CF0
GRH05D00
GRH05D10
GRH05D20
GRH05D30
GRH05D40
GRH05D50
GRH05D60
GRH05D70
GRH05D80
GRH05D90
GRH05DA0
GRH05DB0
GRH05DC0
GRH05DD0
GRH05DE0
GRH05DF0
GRH05E00
GRH05E10
GRH05E20
GRH05E30
GRH05E40
GRH05E50
GRH05E60
GRH05E70
GRH05E80
GRH05E90
GRH05FA0
GRH05FB0
GRH05FC0
GRH05FD0
GRH05FE0
GRH05FF0
GRH06000
GRH06010
GRH06020
GRH06030
GRH06040
GRH06050
GRH06060
GRH06070
GRH06080
GRH06090
GRH060A0
GRH060B0
GRH060C0
GRH060D0
GRH060E0
GRH060F0
GRH06100

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NF#NF&1
Jvary#J
SECOND%K,L<#CHISO
X%J<#XSAVE%J<
DX%J<#-DX%J<
X%I<#XSAVE%I<
2320
C CALL SSWITCH %NSSW,JUMP<
C IF%JUMP-1<2090,2090,2330
C
2330 DX%I<#-DX%I<
ERR%I,J<#0.25*%SECOND%1,1<-SECOND%1,2<-SECOND%2,1<&SECOND%2,2<<
* %DX%I<#DX%J<<
2340 ERR%J,I<#ERR%I,J<
C
C END OF DERIVATIVE COMPUTATION.
2350 IF%NTRACE<2410,2360,2360
2360 WRITE% KW,2370<
2370 FORMAT%41HISIZES OF INCREMENTS TO BE USED BELOW....<
WRITE% KW,2380<%DX%J<,J#1,NV<
2380 FORMAT%/%1X9E13.5<<
WRITE% KW,2390<
2390 FORMAT%////45H MATRIX OF THE SECOND PARTIAL DERIVATIVES.... /<
DO 2400 I#1,NV
2400 WRITE% KW,2380<%ERR%I,J<,J#1,I<
2410 DO 2420 I#1,NV
DO 2420 J#1,I
IF%ERR%I,J<<2420,2430,2420
2420 CONTINUE
GO TO 2450
2430 WRITE% KW,2440<
2440 FORMAT%////46H THE ABOVE MATRIX CONTAINS ONE OR MORE ZEROES. /
* 75H A LARGER VALUE OF -MATRIX- SHOULD BE TRIED, TO SEE IF THEY
* ARE LEGITIMATE. <
C
C *****
C
C INVERT THE MATRIX OF SECOND DERIVATIVES USING THE ALGORITHM SYMINV2
C %ALGORITHM 150, H. RUTISHAUSER, COMMUNICATIONS OF THE A.C.M. 6 %1963<
C P. 67<. RE-USE SOME STORAGE.
C
2450 SGNDDET#1.
DETLOG#0.
DO 2460 J#1,NV
2460 SALVO%J<#1.0
DO 2460 I#1,NV
C
C PERFORM PIVOT SEARCH.
BIGAJJ#0.0
DO 2510 J#1,NV
IF%SALVO%J<<2470,2510,2470
C
C ABER#ABS%ERR%J,J<<
2470 ABER#ERR%J,J<
IF%ABER<2480,2490,2490
2480 ABER#-ABER
2490 IF%ABER-BIGAJJ<2510,2510,2500
2500 BIGAJJ#ABER
K#J
2510 CONTINUE
IF%BIGAJJ<2540,2520,2540
2520 WRITE% KW,2530<
2530 FORMAT%////67H ERROR MATRIX IS SINGULAR. -MATRIX- SHOULD PROBABLY
* BE INCREASED.
GO TO 2120
2540 SALVO%K<#0.0
IF%ERR%K,K<<2550,2550,2560
2550 SGNDDET#-SGNDDET
C
C 2560 DETLOG#DETLOG&ALOG%BIGAJJ</2.303
C 2560 DETLOG#DETLOG&DLOG%BIGAJJ</2.303
C
C PREPARE FOR THE NEXT ELIMINATION STEP.
TRIAL%K<#1.0/ERR%K,K<
ERR%K,K<#0.0
XSAVE%K<#1.0
M#K-1
IF%M<2600,2600,2570
2570 DO 2590 J#1,M
XSAVE%J<#ERR%K,J<
TRIAL%J<#ERR%K,J<*TRIAL%K<
IF%SALVO%J<<2520,2590,2580
2580 TRIAL%J<#-TRIAL%J<
2590 ERR%K,J<#0.0
2600 M#K&1
IF%M-NV<2610,2610,2650
2610 DO 2640 J#M,NV

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GRH06110
GRH06120
GRH06130
GRH06140
GRH06150
GRH06160
GRH06170
GRH06180
GRH06190
GRH061A0
GRH061B0
GRH061C0
GRH061D0
GRH061E0
GRH061F0
GRH06200
GRH06210
GRH06220
GRH06230
GRH06240
GRH06250
GRH06260
GRH06270
GRH06280
GRH06290
GRH062A0
GRH062B0
GRH062C0
GRH062D0
GRH062E0
GRH062F0
GRH06300
GRH06310
GRH06320
GRH06330
GRH06340
GRH06350
GRH06360
GRH06370
GRH06380
GRH06390
GRH063A0
GRH063B0
GRH063C0
GRH063D0
GRH063E0
GRH063F0
GRH06400
GRH06410
GRH06420
GRH06430
GRH06440
GRH06450
GRH06460
GRH06470
GRH06480
GRH06490
GRH064A0
GRH064B0
GRH064C0
GRH064D0
GRH064E0
GRH064F0
GRH06500
GRH06510
GRH06520
GRH06530
GRH06540
GRH06550
GRH06560
GRH06570
GRH06580
GRH06590
GRH065A0
GRH065B0
GRH065C0
GRH065D0
GRH065E0
GRH065F0
GRH06600
GRH06610
GRH06620
GRH06630
GRH06640

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      XSAVE%J<#ERR%J,K<
      IF%$ALVO%J<<2520,2620,2630
2620 XSAVE%J<#-XSAVE%J<
2630 TRIAL%J<#-ERR%J,K<*TRIAL%K<
2640 ERR%J,K<#0.0
C      PERFORM THE NEXT ELIMINATION STEP.
2650 DO 2660 J#1,NV
      DO 2660 K#J,NV
2660 ERR%K,J<#ERR%K,J<&XSAVE%J<*TRIAL%K<
C      * * * * *
C      PRINT THE ERRORS AND CORRELATIONS, AND TERMINATE.
C      IF%SGNDET<2670,2690,2690
2670 WRITE% KW,2680<
2680 FORMAT%////75H ERROR MATRIX IS NEGATIVE DEFINITE. -MATRIX- SHOULD
      * PROBABLY BE DECREASED. <
2690 IF%NTRACE<2720,2700,2700
2700 WRITE%KW,2710<DETLOG,SGNDET
2710 FORMAT%////39H LOG10OF%DETERMINANT OF ABOVE MATRIX< # E12.5,10X
      * 22HSIGN OF DETERMINANT # E8.1<
C      THE ERROR MATRIX IS TWICE THE INVERSE OF
C      THE MATRIX OF SECOND DERIVATIVES.
2720 DO 2790 I#1,NV
      DO 2730 J#1,I
      ERR%I,J<#ERR%I,J<#2.0
2730 ERR%J,I<#ERR%I,J<
C      XSAVE%I<#SIGN%$QRT%ABS%ERR%I,I<<<,ERR%I,I<<<
      ABER#ERR%I,I<
      IF%ABER<2740,2790,2750
2740 ABER#-ABER
C2750 ABER#SQRT %ABER<
2750 ABER#DSQRT%ABER<
      IF%ERR%I,I<<2760,2770,2790
2760 ABER#-ABER
2770 WRITE% KW,2780<ERR%I,I<
2780 FORMAT% ///50H NEGATIVE OR ZERO MEAN SQUARE ERROR ENCOUNTERED...
      * 3XE15.8/39H -MATRIX- SHOULD PROBABLY BE DECREASED. ////<
2790 XSAVE%I<#ABER
      IF%NTRACE<2130,2800,2800
2800 WRITE% KW,2810<
2810 FORMAT%////20H STANDARD ERRORS... <
      WRITE% KW,2380<%XSAVE%J<,J#1,NV<
      IF%NV-1<2120,2120,2820
2820 WRITE% KW,2830<
2830 FORMAT%////45H LOWER TRIANGLE OF THE CORRELATION MATRIX.... /<
      DO 2880 I#2,NV
      IM#I-1
      DO 2870 J#1,IM
      DENOM#XSAVE%I<*XSAVE%J<
      IF%DENOM<2850,2840,2860
2840 TRIAL%J<#0.
      GO TO 2870
2850 DENOM#-DENOM
2860 TRIAL%J<#ERR%I,J</DENOM
2870 CONTINUE
2880 WRITE% KW,2380<%TRIAL%J<,J#1,IM<
      GO TO 2120
      END
      BLOCK DATA
C
C      BLOCK DATA SUBPROGRAM FOR STEPIT, SIMPLEX, AND STP.
C      J. P. CHANDLER, F.S.U. PHYSICS DEPT.
C
      COMMON /FRODO/ NFMAX,NFLAT,JVARY,NEXTRA
      COMMON/ HISTO / ICURVE,CRVMAX,ABE%102<,BIN%102<
      DATA NFMAX/1000000/,NFLAT/1/,NEXTRA/0/
      DATA ICURVE/0/,CRVMAX/0./
      END
/*
//

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GRH06650
GRH06660
GRH06670
GRH06680
GRH06690
GRH066A0
GRH066B0
GRH066C0
GRH066D0
GRH066E0
GRH066F0
GRH06700
GRH06710
GRH06720
GRH06730
GRH06740
GRH06750
GRH06760
GRH06770
GRH06780
GRH06790
GRH067A0
GRH067B0
GRH067C0
GRH067D0
GRH067E0
GRH067F0
GRH06800
GRH06810
GRH06820
GRH06830
GRH06840
GRH06850
GRH06860
GRH06870
GRH06880
GRH06890
GRH068A0
GRH068B0
GRH068C0
GRH068D0
GRH068E0
GRH068F0
GRH06900
GRH06910
GRH06920
GRH06930
GRH06940
GRH06950
GRH06960
GRH06970
GRH06980
GRH06990
GRH069A0
GRH069B0
GRH069C0
GRH069D0
GRH069E0
GRH069F0
GRH06A00
GRH06A10
GRH06A20
GRH06A30
GRH06A40
GRH06A50
GRH06A60
GRH06A70
GRH06A80
GRH06A90
GRH06AA0

```

[illegible]

THIS PROGRAM GENERATES A TEST ARC OF VARIABLE LENGTH IN
CARTESIAN COORDINATES, PROJECTS AND TRANSFORMS TO DATA BASE
COORDINATES AND COMPARES DIRECT AND INTERPOLATED VALUES FOR
INTERMEDIATE POINTS ON THE ARC.

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E-20

E.6 SUBROUTINES USED FOR MAPPING A POINT IN CARTESIAN SPACE INTO DATA BASE COORDINATES

```

C      SUBROUTINE QTRAN(COORD,X,Y,IFACE)
C
C      THIS SUBROUTINE TAKES AS INPUT THE CARTESIAN COORDINATE ARRAY
C      (COORD) AND RETURNS DATA BASE COORDINATES (X AND Y) AND THE
C      FACE NUMBER (IFACE) OF THE X,Y SYSTEM
C
C      PROGRAMMER - E. MICHAEL O'NEILL
C                  COMPUTER SCIENCES CORPORATION
C                  8728 COLESVILLE RD. SILVER SPRING, MD.
C
C      COMMON /TRACOM/ RS,R0,RS0,R4,GAMMA,OMGAM,DELTA,OMEGA,
1      COO,C10,C01,C11,C20,C02,D0,D1,D2
1      DIMENSION COORD(3), C(3), ROT(3,6), IROT(3,6)
1      DATA ROT/1.0,1.0,1.0, -1.0,1.0,-1.0, -1.0,1.0,1.0,
1      1.0,1.0,-1.0, -1.0,-1.0,1.0, -1.0,1.0,-1.0/
1      DATA IROT/2,3,1,2,3,1,1,3,2,1,3,2,1,2,3,1,2,3/
1      DATA OFFSET/2048.0/
C      DETERMINE FACE NUMBER BY FINDING LARGEST (ABS) COMPONENT
      CMAX=ABS(COORD(1))
      J=1
      DO 10 I=2,3
      IF(CMAX.LT.(ABS(COORD(I)))) J=I
      CMAX=ABS(COORD(J))
10     CONTINUE
      IFACE=J*2
      IF(COORD(J).GE.0.0) IFACE=IFACE-1
C      INTERCHANGE CARTESIAN COMPONENTS TO GET TO FACE SYSTEM
      DO 20 I=1,3
C      20 C(I)=COORD(IROT(I,IFACE))*ROT(I,IFACE)
C      PROJECT TO PSI, EIA SYSTEM
      PRJ=R0/C(3)
      P=C(1)*PRJ
      E=C(2)*PRJ
C      TRANSFORM TO X,Y
      X=FMAP(P,E)/R0*OFFSET+OFFSET
      Y=FMAP(E,P)/R0*OFFSET+OFFSET
      RETURN
      END

```

C
C
C
C
C

FUNCTION FMAP(A,B)

THIS FUNCTION PERFORMS THE INVERSE TRANSFORMATION (F STAR)

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COMMON /TRACOM/ RS,R0,RSQ,R4,GAMMA,OMGAM,DELTA,OMEGA,
C00,C10,C01,C11,C20,C02,D0,D1,D2

1 ASQ=A*A
A3=A*ASQ
A4=ASQ*ASQ
BSQ=B*B
B4=BSQ*BSQ
RMA=RSQ-ASQ
FMAP=A*GAMMA+A3*(OMGAM/RSQ)+A*BSQ*RMA*(DELTA+(RSQ-BSQ)*
1 (C00+C10*ASQ+C01*BSQ+C11*ASQ*BSQ+C20*A4+C02*B4))+
2 A3*RMA*(OMEGA+RMA*(D0+D1*ASQ+D2*A4))

RETURN

END

BLOCK DATA

DATA INITIALIZATION FOR FMAP

C
C

COMMON /TRACOM/ RS,R0,RSQ,R4,GAMMA,OMGAM,DELTA,OMEGA,
C00,C10,C01,C11,C20,C02,D0,D1,D2

1 DATA RS,R0,RSQ,R4/1.0,0.577350,0.333333,0.111111/
DATA GAMMA,OMGAM,DELTA,OMEGA/1.381976,-.381976,-.834527,0.056318/
DATA C00,C10,C01,C11,C20,C02/4.800983,23.47334,-40.99963,
325.4193,-318.1992,-9.85862/
1 DATA D0,D1,D2/-12.80531,59.46511,-256.5819/
END

E.7 SUBROUTINES USED FOR SIMULATING THE FAST-FILLING METHOD

```

SUBROUTINE SCAN1(INBASE,NSL,NBL)
  THIS SUBROUTINE SIMULATES THE STORAGE OF DATA IN THE DATA BASE
  ON A SINGLE INTERPOLATION BLOCK BASIS.
  INTERPOLATION ALONG AND BETWEEN SCAN LINES TAKES PLACE USING
  VECTOR COMPONENTS INPUTTED (IPZ,IEZ,IDP,IDE,JDP,JDE).
  THE SERIAL ADDRESS IS CALCULATED USING A TABLE LOOK UP AND
  THE RECORD NUMBER IS DETERMINED BY A SHIFT OF THE SERIAL ADDRESS.

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  LOGICAL FAILW
  LOGICAL*1 INDATA,IODATA
  INTEGER SHFTL,SHFTR
  COMMON/DATCOM/ INDATA(81920), IODATA(24576)
  COMMON /INDCOM/ INDX(4096), INDY(4096), ISHFT, NMIL
  COMMON /SCNCOM/ IPZ, IEZ, IDP, IDE, JDP, JDE, JSIZE
  DATA LREC/-1/
  KLOC=INBASE
  DO 20 IBL=1,NBL
    JLOC=KLOC
    IP=IPZ
    IE=IEZ
    DO 10 ISL=1,NSL
      I=IP/ISHFT
      J=JP/ISHFT
      KEY=INDX(I)+INDY(J)
      IREC=SHFTR(KEY,6)
      IF (IREC.EQ.LREC) GO TO 5
      LREC=IREC
      CALL IOMNGR (IREC,IOBASE,FAILW)
5     IF (FAILW) GO TO 9
      ILOC=KEY-SHFTL (IREC,6)
      IDUM=IOBASE+ILOC
      INDATA (IOBASE+ILOC)=INDATA (JLOC)
9     IP=IP+IDP
10    IE=IE+IDE
      KLOC=KLOC+JSIZE
      IPZ=IPZ+JDP
20    IFZ=IFZ+JDE
      RETURN
    END
  SUBROUTINE IOMNGR (IREC,IOBASE,FAILW)
    LOGICAL FAILW
    IOBASE=0
    FAILW=.FALSE.
    RETURN
  END
// EXEC LOADER,REGION=200K,PARM=' SIZE=200000'
//

```

E.8 SUBROUTINES USED FOR TESTING I/O HANDLING METHOD

```

SUBROUTINE IOMNGR(IKEY,IOBASE,FAILW)
  THIS SUBROUTINE CONTROLS DATA BASE INPUT/OUTPUT
  THIS SUBROUTINE TAKES AS INPUT THE SERIAL ADDRESS OF A
  RECORD REQUIRED FOR PROCESSING, COMPARES THE RECORD NUMBER
  WITH A LIST OF RECORDS AVAILABLE IN CORE BUFFER AND FETCHES
  NEW RECORDS WHEN NEEDED.
  THE CORE BUFFER IS CONTROLLED BY A PUSH DOWN STACK,
  WHEN A NEW RECORD IS REQUIRED THE OLDEST RECORD IN THE BUFFER
  IS RETURNED TO THE DATA BASE AND REPLACED BY THE REQUESTED
  RECORD. THE BASE ADDRESS OF THE REQUESTED RECORD IS RETURNED
  TO THE CALLING PROGRAM IN IOBASE.
  IOMNGR ALSO RETURNS THE WINDOW FLAG TO INDICATE PRESENCE
  OR ABSENCE OF THE REQUESTED RECORD IN THE DATA BASE.

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  LOGICAL FAILW, FAIL(3,6)
  DIMENSION INDEX(3,6), LINDEX(3)
  EQUIVALENCE (FAIL(1,1),INDEX(1,1))
  DATA NSTAK/0/, MSTAK/6/
  DATA INDEX /-1,6,0,-1,5,0,-1,4,0,-1,3,0,-1,2,0,-1,1,0/

  ON FIRST ENTRY IMMEDIATELY GET REQUESTED RECORD
  IF(NSTAK.EQ.0) GO TO 25
  TEST REQUEST RECORD NUMBER AGAINST RECORDS IN CORE
  DO 20 I=1,NSTAK
  JKEY=LINDEX(2,I)
  BRANCH IF A MATCH IS FOUND
  IF(IKEY.EQ.INDEX(1,I)) GO TO 30
20 CONTINUE
  BRANCH IF STACK IS NOT YET FULL
  IF(NSTAK.LT.MSTAK) GO TO 25
  ENTER REQUESTED RECORD INTO STACK
  CALL PUSHD(INDEX,LINDEX,MSTAK,IKEY)
  JKEY=LINDEX(2)
  RETURN OLDEST RECORD TO DATA BASE
  CALL PUTREC(LINDEX(1),LINDEX(2),FAILW)
  READ NEW RECORD INTO SPACE VACATED
  CALL GETREC(INDEX(1,1),INDEX(2,1),FAILW)
  FAIL(3,JKEY)=FAILW
  GO TO 30
  ENTER AND FETCH ONLY UNTIL STACK IS FULL
25 NSTAK=NSTAK+1
  JKEY=NSTAK
  CALL PUSHD(INDEX,LINDEX,MSTAK,JKEY)
  CALL GETREC(IKEY,JKEY,FAILW)
  FAIL(3,JKEY)=FAILW
  SET BASE ADDRESS AND WINDOW FAILURE FLAG BEFORE RETURNING
30 INBASE=(JKEY-1)*1024
  FAILW=FAIL(3,JKEY)
  RETURN
  END

```


SUBROUTINE WINDOW(NREC,MREC,FAILW)

[illegible]C
C
C

CCC

CCC

C
C
C
C
C
C
C

SUBROUTINE GRAY3(NGRA,I128)

THIS SUBROUTINE CREATES A GRAY SCALE PLOT OF A 128 X 128
INPUT ARRAY ON THE PRINTER. GRAY3 OVERPRINTS UP TO TWO TIMES,
FOR TONES RANGING FROM WHITE (1) TO BLACK (16).

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```

LOGICAL*1 I128(128,128)
LOGICAL LS
DIMENSION ISYM(16,3), NSYM(16), IOUT(128,3)
EQUIVALENCE (IS,LS)
DATA NS/16/, NL/3/, IB/1H /, IP/1H+/
DATA ISYM/
1 1H ,1H.,1H.,,1H=,1HU,1HX,1H#,1H8,1HM,1HO,1HO,1HO,1HO,1HO,1HO,1HO,
2 1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H=,1HI,1H+,1H*,1H*,1H*,
3 1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H ,1H- ,1HX,1HM/
DATA NSYM /1,1,1,1,1,1,1,1,1,1,2,2,2,2,3,3,3/
DO 60 J=1,128
  IPMAX=1
  DO 30 I=1,128
    LS=I128(I,J)
    IF (IS.LT.1) IS=1
    IF (IS.GT.NS) IS=NS
    DO 20 IL=1,NL
20  IOUT(I,IL)=ISYM(IS,IL)
    IF (NSYM(IS).GT.IPMAX) IPMAX=NSYM(IS)
30  CONTINUE
    ICC=IB
    DO 50 IL=1,IPMAX
      WRITE(NGRA,40) ICC,(IOUT(I,IL),I=1,128)
40  FORMAT(A1,2X,128A1)
50  ICC=IP
60  CONTINUE
    RETURN
  END

```

REFERENCES

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2. Goldstein, H., Classical Mechanics. Reading, Massachusetts: Wesley Publishing Co., June 1959